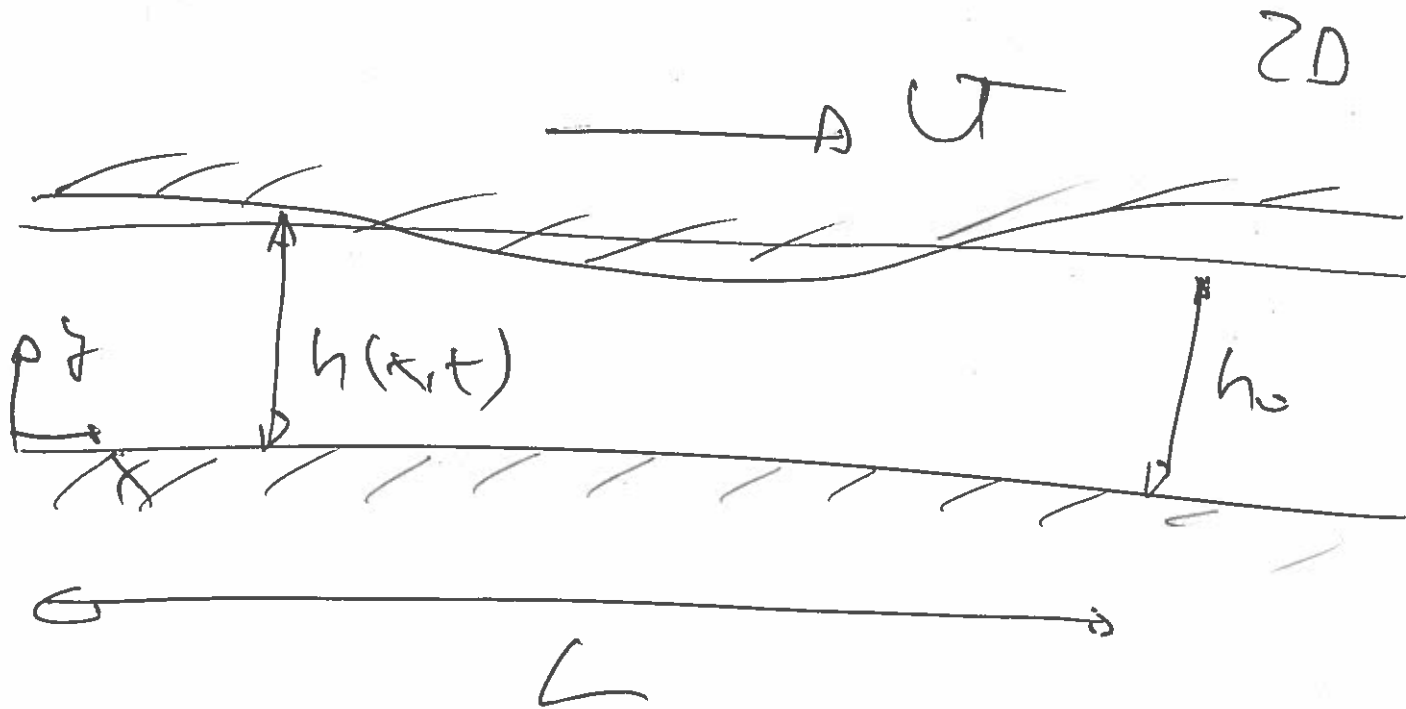


# Further example for scaling

## §9 Lubrication theory



Gap narrow & gently varying  
 $h_0 \ll L$ ;  $\frac{h_0}{L} \ll 1$

Scale:

$$x = L \tilde{x}$$

$$y = h_0 \tilde{y}$$

$$u = U \tilde{u}$$

$$v = V \tilde{v}$$

$$t = \frac{L}{U} \tilde{t}$$

$$p = P \tilde{p}$$

$P$  &  $V$  unknown.

Continuity:

(2)

$$\frac{U}{L} \frac{\partial \tilde{\psi}}{\partial \tilde{x}} + \frac{V}{h_0} \frac{\partial \tilde{\psi}}{\partial \tilde{y}} = 0$$

$$U \frac{h_0}{L} \frac{\partial \tilde{\psi}}{\partial \tilde{x}} + V \frac{\partial \tilde{\psi}}{\partial \tilde{y}} = 0$$

These terms only balance  
if  $V = U \frac{h_0}{L}$

So  $V \ll U$  (as expected)

N. St:

$$\begin{aligned} & \int \left( \frac{U^2}{L} \frac{\partial \tilde{\psi}}{\partial \tilde{x}} + \frac{U^2}{L} \tilde{\psi} \frac{\partial \tilde{\psi}}{\partial \tilde{x}} + \frac{U^2 h_0}{L} \tilde{\psi} \frac{\partial \tilde{\psi}}{\partial \tilde{y}} \right) = \\ & = -\frac{1}{L} \frac{\partial \tilde{\psi}^2}{\partial \tilde{x}} + \mu \left( \frac{U}{L^2} \frac{\partial \tilde{\psi}^2}{\partial \tilde{x}} + \frac{U}{h_0^2} \frac{\partial \tilde{\psi}^2}{\partial \tilde{y}} \right) \end{aligned}$$

$$\frac{\rho U^2}{L} \frac{\partial \tilde{u}}{\partial \tilde{x}} = -\frac{\rho}{L} \frac{\partial \tilde{p}}{\partial \tilde{x}} + \left( \frac{\mu U}{h_0^2} \right) \left( \frac{h_0}{L} \frac{\partial^2 \tilde{u}}{\partial \tilde{x}^2} + \frac{\partial^2 \tilde{u}}{\partial \tilde{y}^2} \right) \quad (3)$$

$$Re \left( \frac{h_0}{L} \right) \ll 1$$

$$\frac{\rho U h_0}{\mu} \left( \frac{h_0}{L} \right) \frac{\partial \tilde{u}}{\partial \tilde{x}} = -\frac{\rho}{\left( \frac{\mu U}{h_0} \right) \left( \frac{h_0}{L} \right)} \frac{\partial \tilde{p}}{\partial \tilde{x}} + \frac{\partial^2 \tilde{u}}{\partial \tilde{y}^2}$$

Re based on  $h_0$ .

Note that in this geometry it is the product of Re &  $\frac{h_0}{L}$  that determines the size of the non-lin. terms.

They can be neglected if

$$Re \left( \frac{h_0}{L} \right) \ll 1.$$

Balancing the remaining terms determines  $\rho$ .

$$P = \frac{\mu U}{h_0} \frac{1}{\left(\frac{h_0}{4}\right)}$$

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$$0 = -\frac{\partial p}{\partial x} + \frac{\partial^2 u}{\partial y^2}$$

Similarly  $y$ -comp. N.S.:

$$\frac{\partial^2 p}{\partial y^2} = 0$$

(EXERCISE)

or in dimensional form

$$0 = -\frac{\partial p}{\partial x} + \mu \frac{\partial^2 u}{\partial y^2} \quad (1)$$

$$0 = -\frac{\partial p}{\partial y} \quad (2)$$

Parallel flow eqns!

The gentle slope of the  $\zeta$  wall means that locally the flow behaves like parallel flow through an infinitely long channel of the same width.

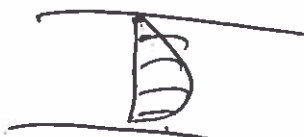

BC:  $u(y=0) = 0$   
 $u(y=h(x,t)) = U$

Since (2):  $p(x,y) = p(x)$

into (1):  $\frac{\partial p}{\partial x} = \mu \frac{\partial^2 u}{\partial y^2}$

$u = \frac{1}{2\mu} \frac{\partial p}{\partial x} y^2 + Ay + B \quad (+ \text{BC}):$

$u(x,y,t) = \underbrace{\frac{1}{2\mu} \frac{\partial p}{\partial x} (y^2 - \overbrace{h(x,t)}^{\text{h}(x,t)})}_{\text{pressure-driven}} + U \underbrace{\frac{y}{h}}_{\text{shear flow}}$

Also: what is  $\frac{dp}{dx}$  ? 16