

Continuity eqn:

(1)

Integral:

$$\int \frac{\partial \rho}{\partial t} dV + \oint \rho \underline{u} \cdot \underline{n} dA = 0$$

Differential:

$$\frac{\partial \rho}{\partial t} + \text{div}(\rho \underline{u}) = 0$$

$\rho = \rho(x_k, t)$  density  $\left[ \frac{\text{kg}}{\text{m}^3} \right]$

$$\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x_i} (\rho u_i) = 0$$

$$\frac{\partial \rho}{\partial t} + u_i \frac{\partial \rho}{\partial x_i} + \rho \frac{\partial u_i}{\partial x_i} = 0$$

$\frac{D\rho}{Dt}$  = rate of change of density of a fluid particle

For an incompressible fluid

$$\frac{D\rho}{Dt} = 0$$

for such fluids:

(2)

$$\frac{\partial u_i}{\partial x_i} = \operatorname{div} \underline{u} = 0$$

This is a purely kinematic constraint!

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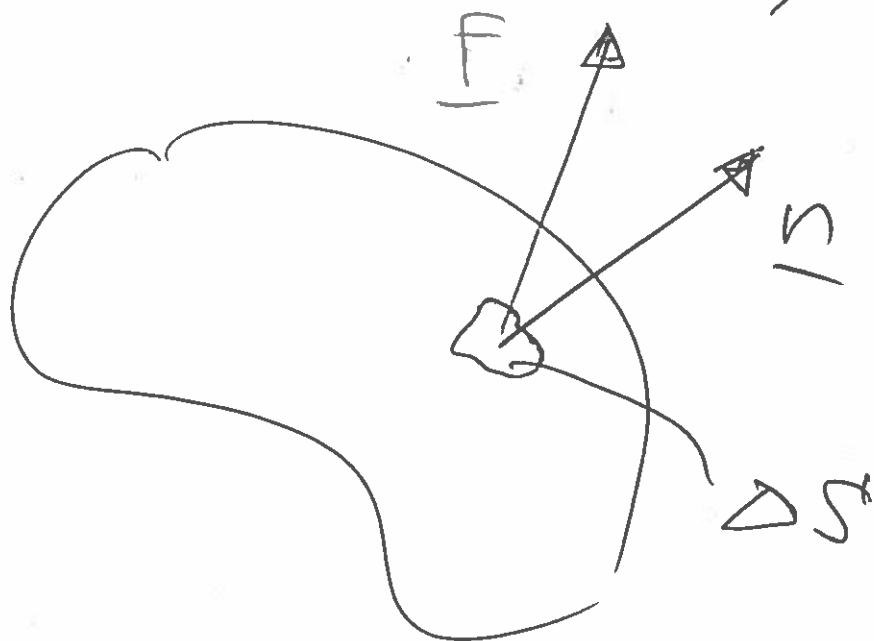
§ n+1 Stress, Cauchy's eqn.  
the Navier-Stokes eqns

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Idea: Use Newton's 2<sup>nd</sup> law for the fluid to determine an ~~eqn~~ eqn for the evolution of u.

① The concept of stress/  
traction

Consider a finite blob of fluid loaded by some distributed force (pressure, shear stress, etc.) (3)



Every patch  $\Delta S$  on the surface (outer unit normal  $\underline{n}$ ) is subject to a resultant force  $\underline{F}$

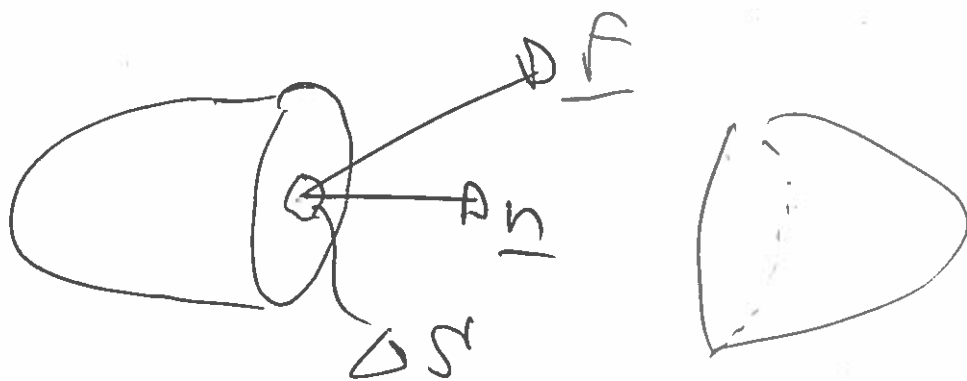
Def: Traction

$$\underline{t} = \lim_{\Delta S \rightarrow 0} \frac{\underline{F}}{\Delta S} \quad \text{vector!}$$

(4)

$\underline{t}$  = force per unit area  
exerted onto the  
fluid.

Similarly: Cut the blob  
along a plane with outer  
unit normal  $\underline{n}$ :



Here  $\underline{F}$  represents the force  
exerted onto  $\Delta S$  by  
the other half of the blob.

Def: Stress

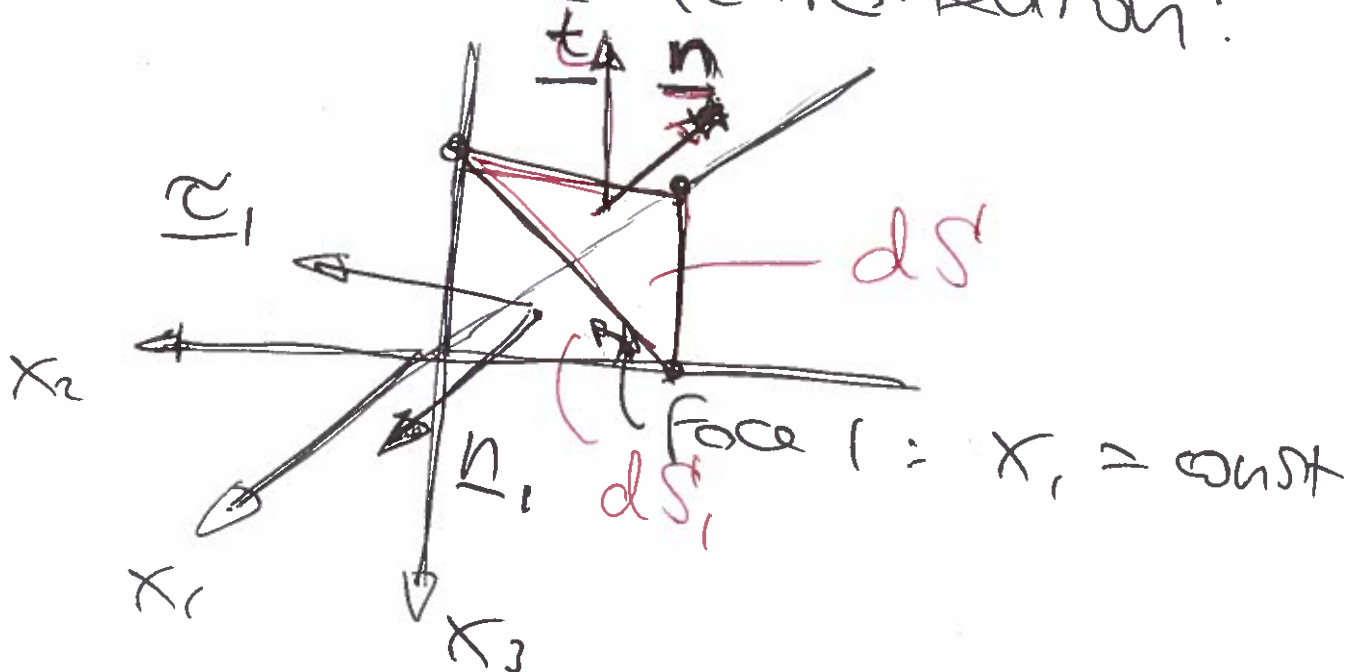
$$\underline{t} = \lim_{\Delta S \rightarrow 0} \frac{\underline{F}}{\Delta S} \quad \text{vector!}$$

Note: Stress depends on  $\underline{S}$

- the position in fluid
- the direction of the "cut", i.e. on  $\underline{n}$ .

## ② The stress tensor

To examine dependence of  $\underline{t}$  on  $\underline{n}$  consider an infinitesimal tetrahedron:



$$\underline{n}_1 = \underline{e}_1$$

Face  $i$  is characterized by  $\epsilon$   
 $x_i = \text{const.}$  &  $\underline{n}_i = \underline{e}_i$ .

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Trick: Represent the faces  
(have orientation & an area!)  
by area vectors  $\parallel$  to our  
unit normals & magnitude =  
area.

Then:

$$\underline{n}_i dS_i + \underline{n} dS = 0$$

(EXERCISE)

multiply by  $\underline{n}_j = \underline{e}_j$

$$\underbrace{n_i \cdot \underline{n}_j}_{\delta_{ij}} dS_i + \underbrace{\underline{n} \cdot \underline{e}_j}_{n_j} dS = 0$$

$\hookrightarrow j$ -th comp.  
of  $\underline{n}$

$$dS_j^* = -n_j dS^*$$

(7)

Now: balance of forces

$\Rightarrow$  Sum of all forces has to be zero.

$$\underline{t} dS^* = - \underline{\tau}_j dS_j^*$$

$$\underline{t} dS^* = \underline{\tau}_i n_i dS^*$$

$$\underline{t}_i = \tau_{ij} n_j$$

$\tau_{ij}$  = stress tensor.