

$$\rho \left( \frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) = - \frac{\partial p}{\partial x_i} + \mu \frac{\partial^2 u_i}{\partial x_j^2} \quad (1)$$

$$\frac{\partial u_j}{\partial x_j} = 0$$

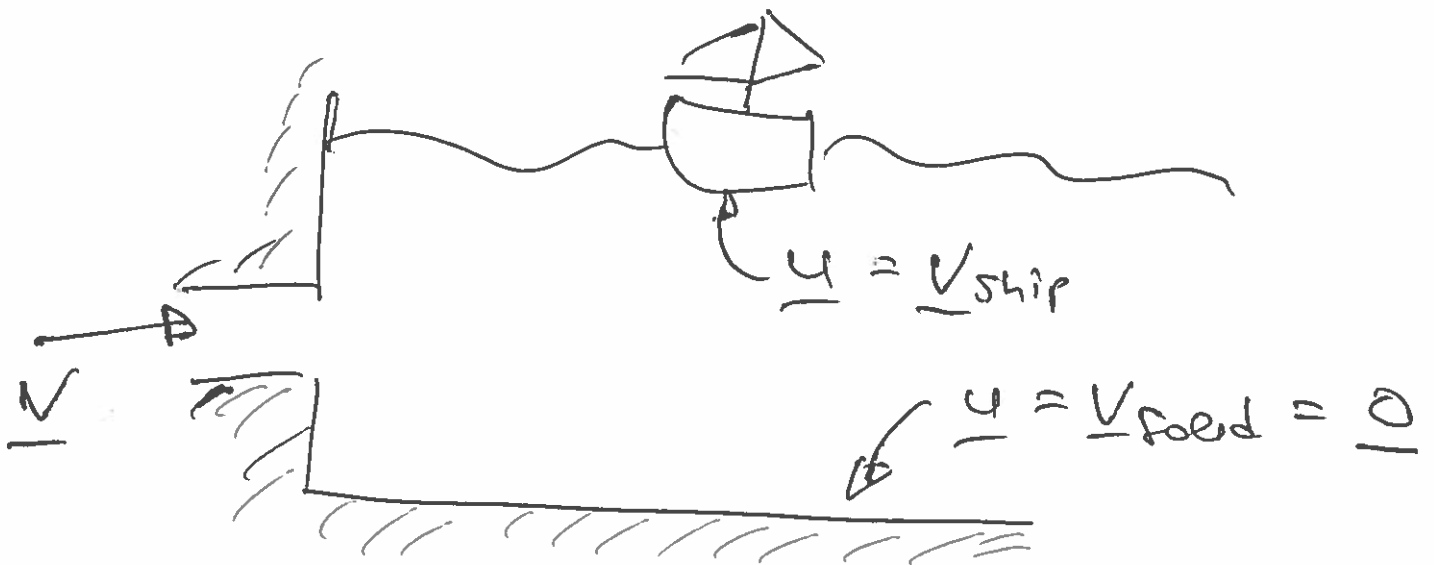
IC:  $\underline{u}(\underline{x}, t=0) = \underline{V}(\underline{x})$  given  
(no IC for pressure!)

BC: Inflow/outflow:

$$\underline{u} = \underline{V} \leftarrow \text{given}$$

solid boundaries "no slip":

$$\underline{u} = \underline{V}_{\text{solid}} \leftarrow \text{given}$$



(iii) on free surfaces

(2)

We need two conditions:

- Kinematic BC
- traction BC.

(a) Kinematic BC

The posn. of the free surface can always be described implicitly

$$F(x, y, z; t) = 0$$

or

$$f(x, y; t) = 0 \quad \text{in 2D}$$

At least locally this can always be inverted to

$$z = h(x, y, t)$$

or

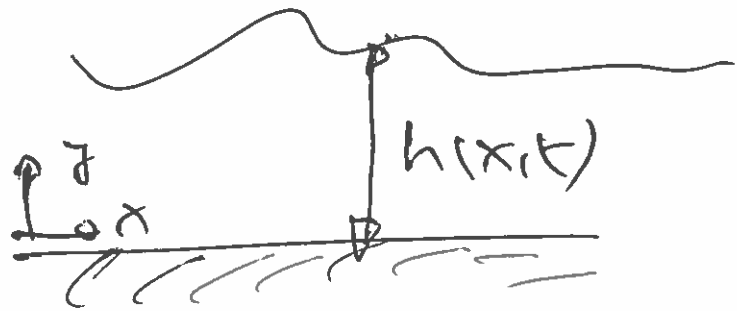
$$y = h(x, t) \quad \text{in 2D}$$

Observation: Fluid particles which form part of the surface always stay on that surface (exception: cusp)

So for  $x_i = x_i^p(t)$ :  $f \equiv 0 \forall t$

$$\Rightarrow \left[ \frac{Df}{Dt} = 0 \right]$$

Example:



$$y / \partial \phi_F = h(x,t)$$

we can use

$$F(x, y, t) = h(x,t) - y = 0$$

Kinematic BC

$$\frac{DF}{Dt} = 0$$

(4)

$$\frac{\partial F}{\partial t} + u \frac{\partial F}{\partial x} + v \frac{\partial F}{\partial y} = 0$$

$$x_1 = u$$

$$x_2 = v$$

$$x_1 = x$$

$$x_2 = y$$

$$\frac{dF}{dt} = \frac{\partial h}{\partial t}$$

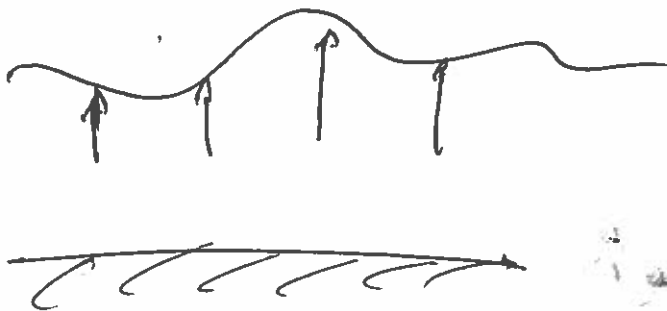
$$\frac{\partial F}{\partial x} = \frac{\partial h}{\partial x}$$

$$\frac{\partial F}{\partial y} = 1$$

$$\frac{DF}{Dt} = \frac{\partial h}{\partial t} + u \frac{\partial h}{\partial x} - v = 0$$

Special case 1:

$u = 0$  (only vertical flow)

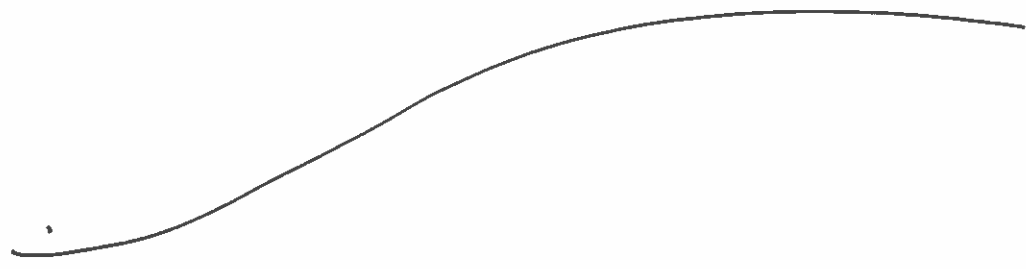


$$\frac{\partial h}{\partial t} = v \quad \checkmark$$

of course!

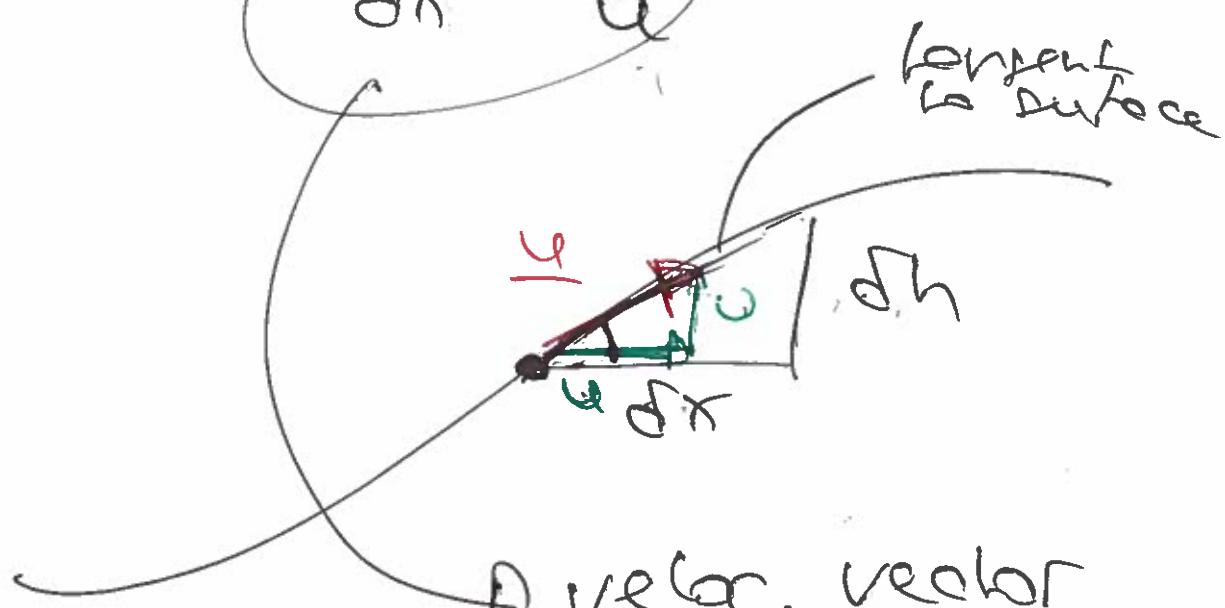
Special case 2:

fixed free surface posn ::  $\frac{\partial}{\partial t} = 0$



$\frac{\partial h}{\partial t} = 0 : u \frac{\partial h}{\partial x} = u$

$\frac{\partial h}{\partial x} = \frac{u}{c}$



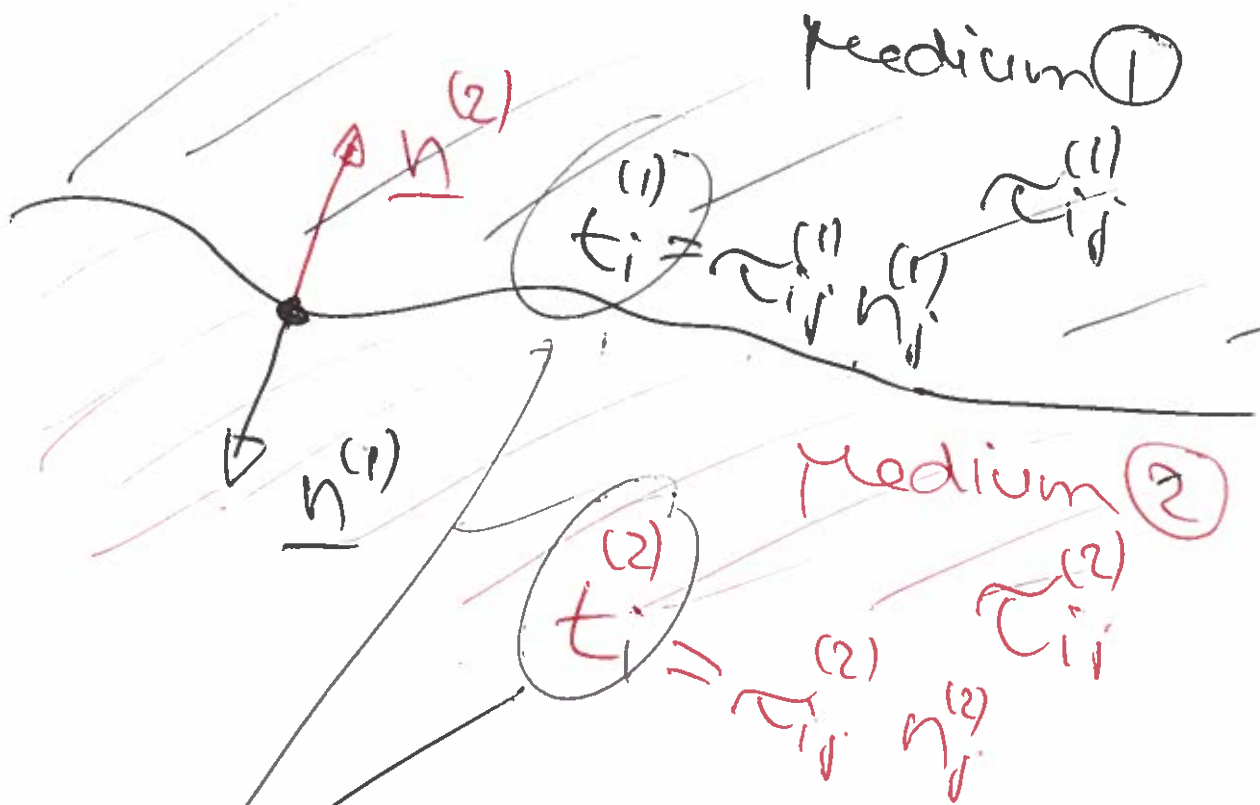
A veloc. vector is tangential to the surface.

of course ✓

# (b) traction BC

(6)

stress must be continuous across the free surface (apart from surface tension effects)



$t_i^{(1)}$  &  $t_i^{(2)}$  are tractions applied onto medium (1) & (2) respectively.

Now: "Action = reaction" (7)

$$\underline{t}^{(1)} = - \underline{t}^{(2)}$$

Also:  $\underline{n}^{(1)} = - \underline{n}^{(2)}$

So:

$$\tau_{ij}^{(1)} n_j = \tau_{ij}^{(2)} n_j$$

(on the boundary)

for any outer unit normal.

Example Hydrostatic pressure state:

$$\tau_{ij} = -p \delta_{ij} :$$

$$\tau_{ij}^{(1)} \delta_{ij} n_j = -p^{(1)} \delta_{ij} n_j = -p^{(2)} \delta_{ij} n_j = \tau_{ij}^{(2)} \delta_{ij} n_j$$

$$-p^{(1)} n_i = -p^{(2)} n_i$$

$$-p^{(1)} \underline{n} = -p^{(2)} \underline{n}$$

$$\underbrace{(p^{(1)} - p^{(2)})}_{=0} \underline{n} = \underline{0}$$

$$p^{(1)} = p^{(2)}$$

✓  
of course

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In the presence of  
Surface tension:

$$\tau_{ij}^{(1)} n_j + \sigma \kappa n_i = \tau_{ij}^{(2)} n_j$$

surface  
tension

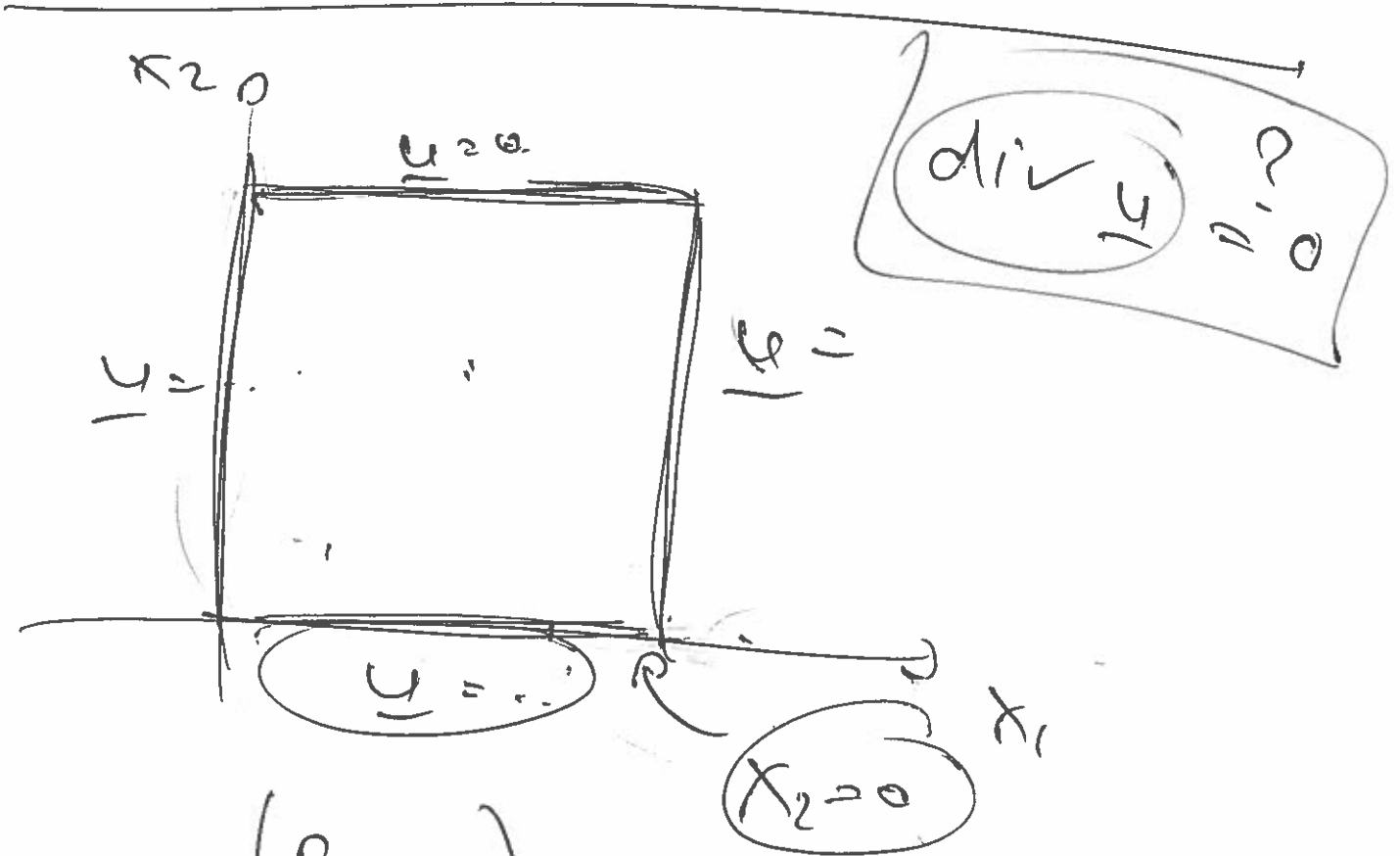
curvature  
of the  
surface:



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$$\text{div } \underline{u} = 0$$

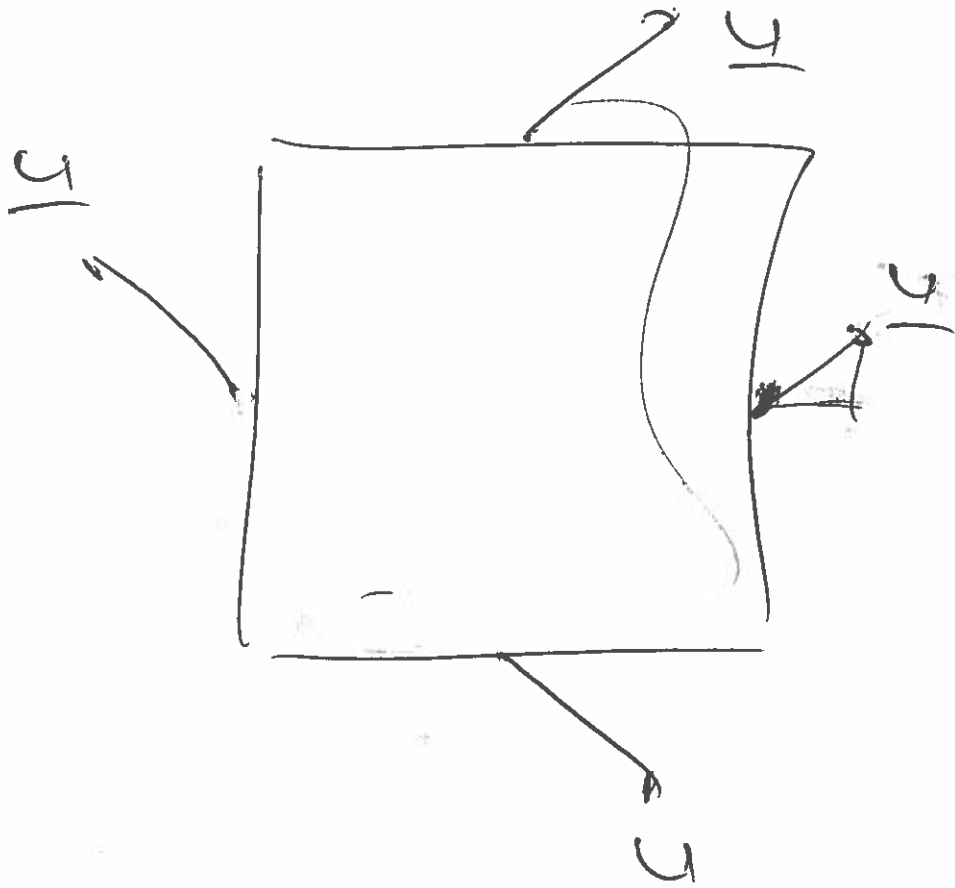
$$\frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} = 0 \Rightarrow A = \frac{1}{3}$$



$$\underline{u} = \begin{pmatrix} 3 \\ 4 + 3x_1^2 \end{pmatrix}$$

$$\text{div } \underline{u} = \frac{\partial}{\partial x_1} 3 + \frac{\partial}{\partial x_2} (4 + 3x_1^2)$$

$$= 0 + 0 = 0$$

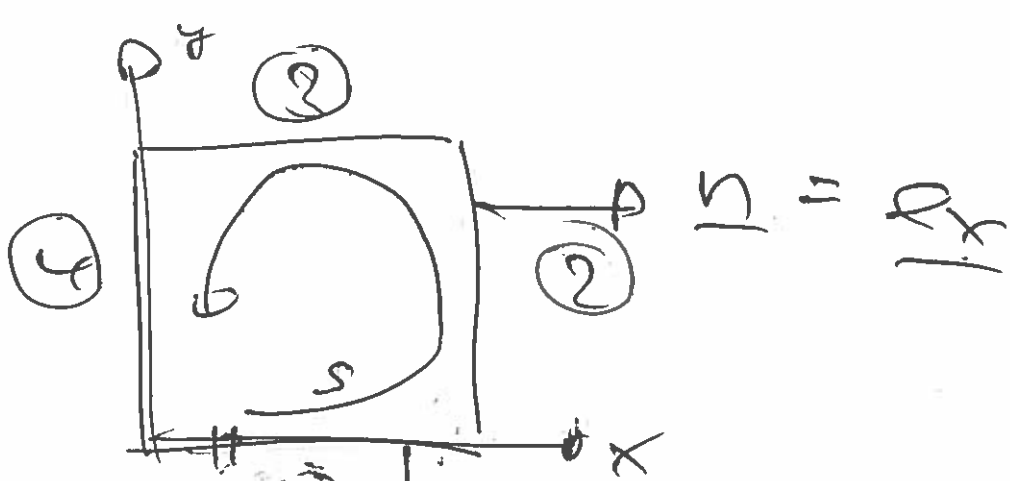


$$\oint \rho \underline{u} \cdot \underline{n} \, dA = \frac{d}{dt} \iiint \rho \, dV$$

Assume fluid is incompressible.

$$\oint \rho \underline{u} \cdot \underline{n} \, dA = 0$$

$$\oint \underline{u} \cdot \underline{n} \, dA \stackrel{\rho \neq 0}{=} 0$$



①

$$\int \frac{y}{|n|} \frac{y}{|n|} ds = \begin{cases} 0 \\ \neq 0 \text{ or} \end{cases}$$

①:  $\frac{y}{|n|} \cdot \frac{y}{|n|} = -(4 + 3x_1^2)$

①  $\int \frac{y}{|n|} \cdot \frac{y}{|n|} ds = \int_{x_1=0}^{-1} -(4 + 3x_1^2) dx_1$

②:  $\int \frac{y}{|n|} \cdot \frac{y}{|n|} ds = \int_{x_2=0}^{-1} (3 + x_2 + x_2^2) dx_2$