

F = resultant force on ΔS

$$\underline{t} = \lim_{\Delta S \rightarrow 0} \frac{F}{\Delta S}$$

stress depends on orientation, \underline{n} .

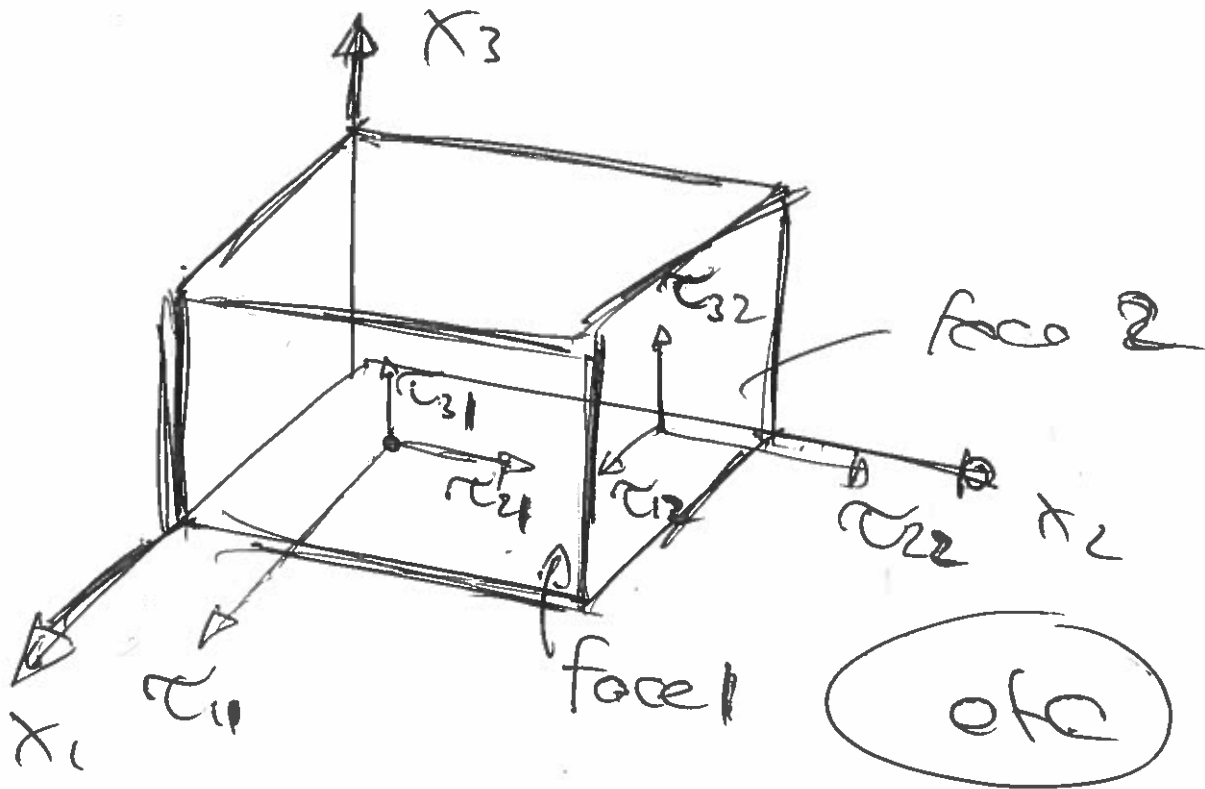
$$t_i = \tau_{ij} n_j$$

$\underbrace{\tau_{ij}}_{\text{stress tensor}}$

= i -th component of stress on face where $x_j = \text{const}$ & outer unit normal points in pos. x_j -direction

Sketch:

(2)

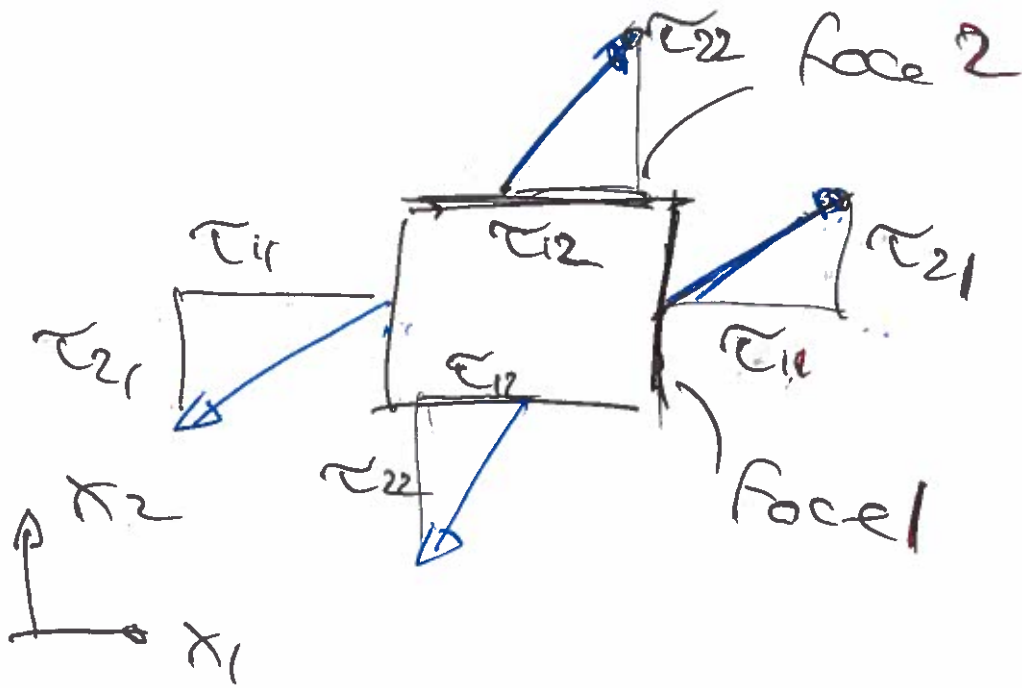


Diagonal entries in τ_{ij}
are normal components
(pressure, tension)
off diagonal entries =
tangential components
= shear stresses

What ~~about~~ about the other
faces? The only difference
is the sign of the outer
unit normal.

2D sketch:

3



Can now express the stress on a face in the fluid in terms of τ_{ij} .

Later we will determine τ_{ij} as a fct. of the fluid's kinematics.

Particular stress states

14

(i) Hydrostatic pressure

$$\tau_{ij} = -p \delta_{ij}$$

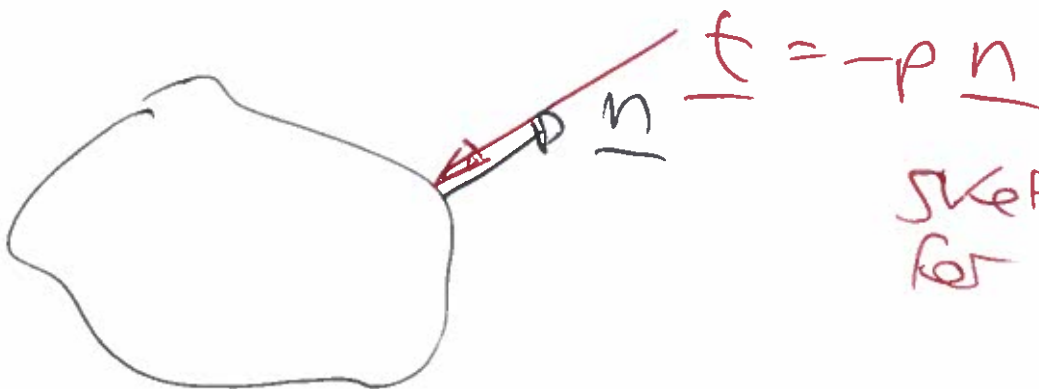
implies that the traction is always normal to the face & uniform in all directions.

Proof:

$$t_i = \tau_{ij} n_j$$

$$t_i = -p \delta_{ij} n_j = -p n_i$$

$$\underline{t} = -p \underline{n}$$



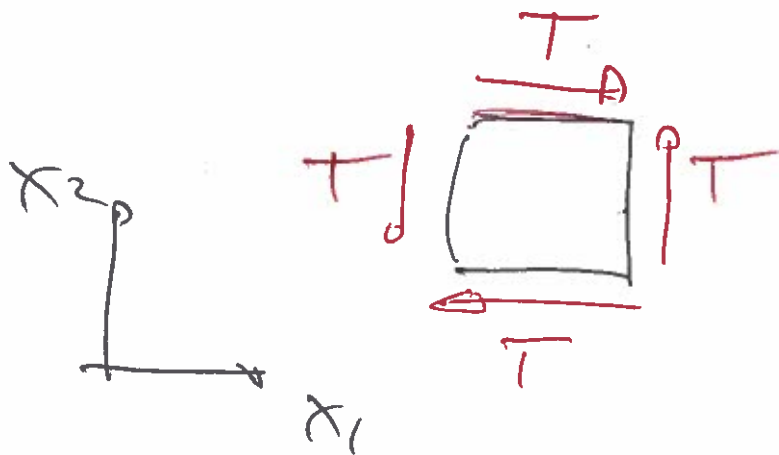
Sketch
for $p > 0$.

Also note: negative normal stress = compression. (5)

(ii) pure shear stress

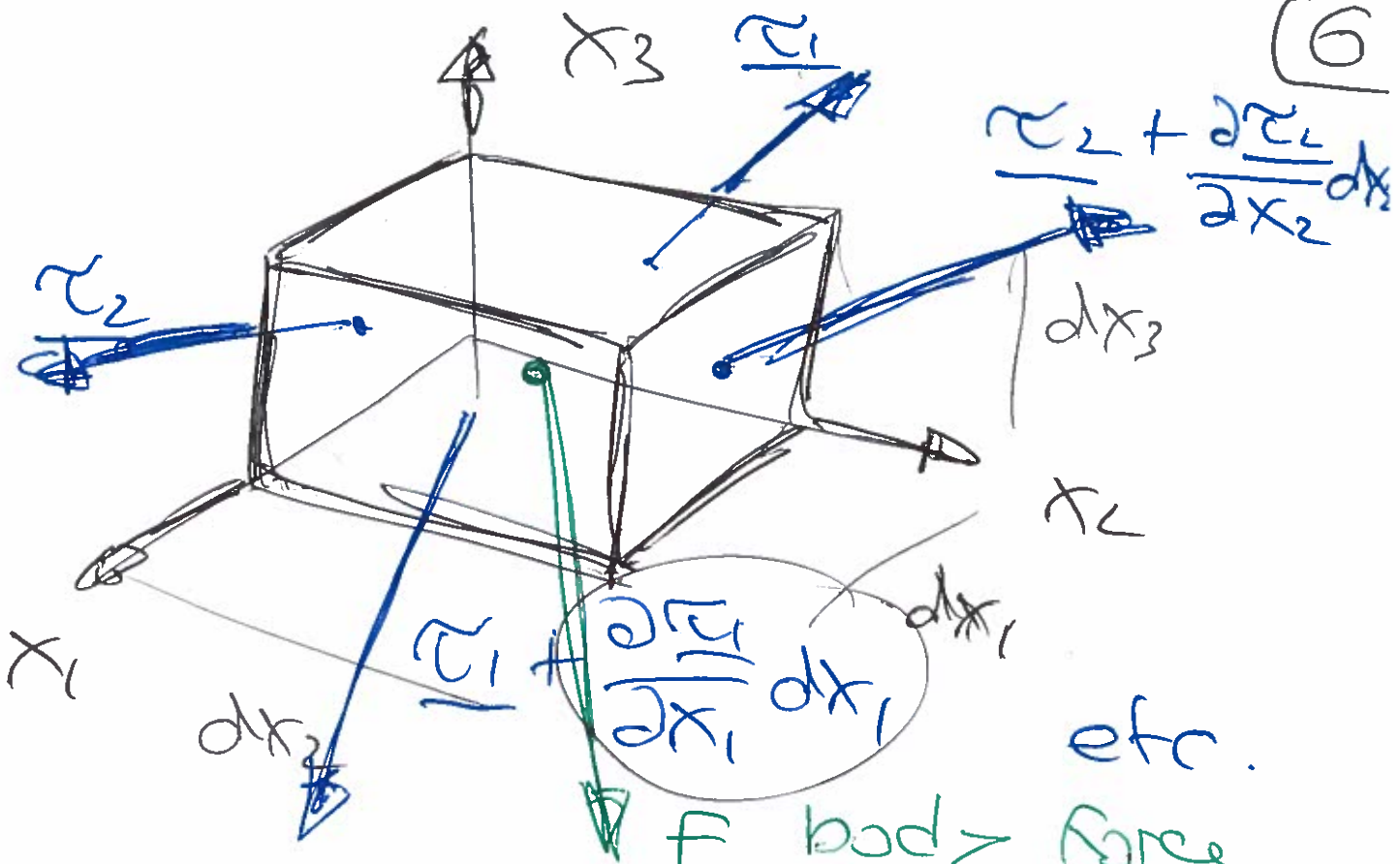
e.g. $\tau_{12} = \tau_{21} = T$

$$\tau_{11} = \tau_{22} = 0$$



3. Equilibrium of forces

" $\sum \text{forces} = \text{mass} \times \text{accel.}$ "
for a small blob of fluid.



Note: contributions from opposite faces cancel, leaving just the increments.

$$\frac{\partial \tau_{(1)}}{\partial x_{(1)}} dx_{(1)} \underbrace{dx_{(2)} dx_{(3)}}_{\text{area}} +$$

$$\frac{\partial \tau_{(2)}}{\partial x_{(2)}} dx_{(2)} \underbrace{dx_{(1)} dx_{(3)}}_{\text{area}} +$$

$$\frac{\partial \tau_{(3)}}{\partial x_{(3)}} dx_{(3)} \underbrace{dx_{(1)} dx_{(2)}}_{\text{area}} +$$

$$\rho \int dx_{(1)} dx_{(2)} dx_{(3)} = \text{Volume}$$

$$\rho \frac{D u}{D t} dx_{(1)} dx_{(2)} dx_{(3)}$$

Summ. conv. & def. of π_{ij} (7)

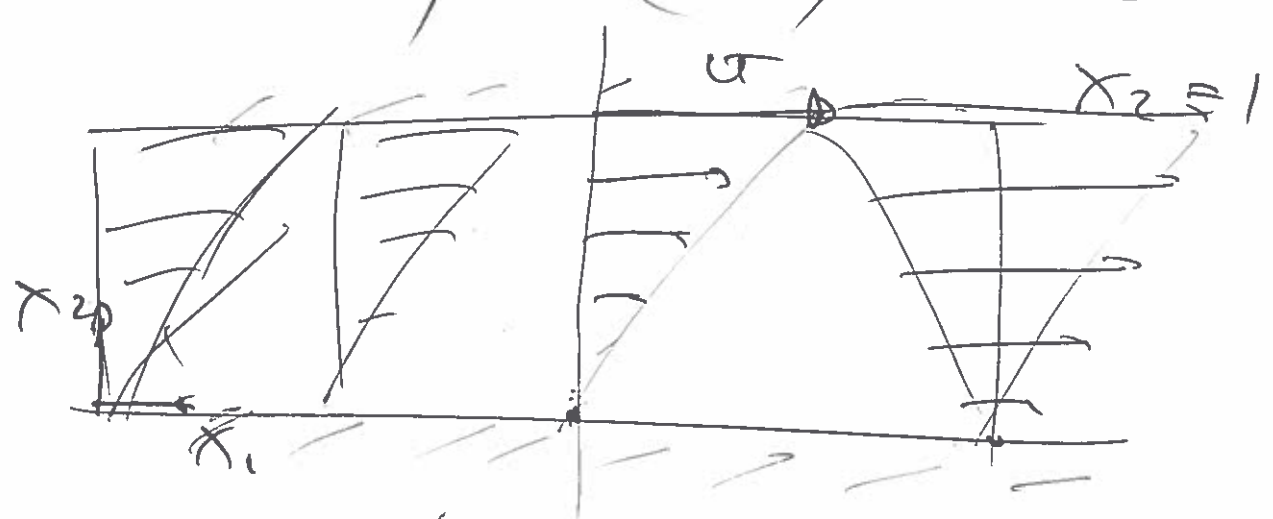
$$\frac{\partial \pi_{ij}}{\partial x_j} + g F_i = g \frac{D u_i}{D t}$$

Cauchy's eqn!

X-CUTS

$$u = \begin{pmatrix} u_1 \\ u_2 \end{pmatrix} = \begin{pmatrix} u x_2 \\ 0 \end{pmatrix} \quad u > 0$$

(1)

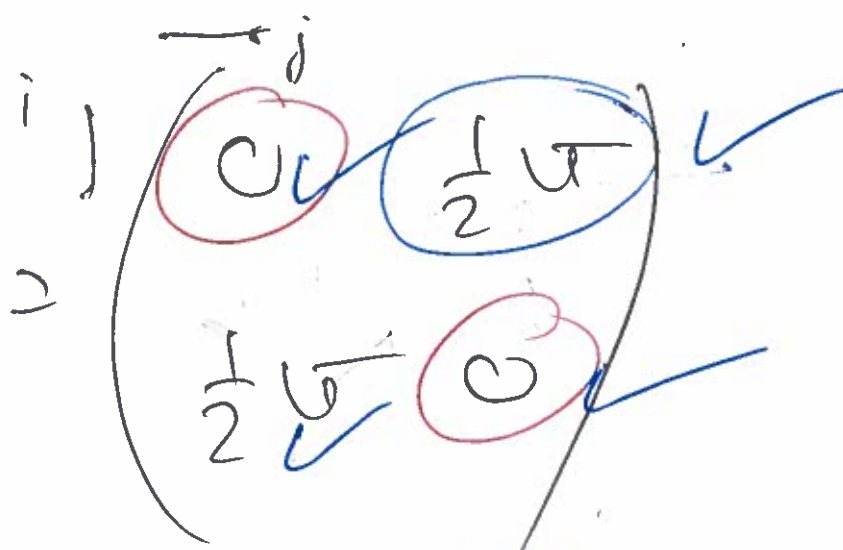


$$\epsilon_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \quad \epsilon_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} - \frac{\partial u_j}{\partial x_i} \right)$$

$$[\epsilon_{ij}] = \begin{pmatrix} \epsilon_{11} & \epsilon_{12} \\ \epsilon_{21} & \epsilon_{22} \end{pmatrix}$$

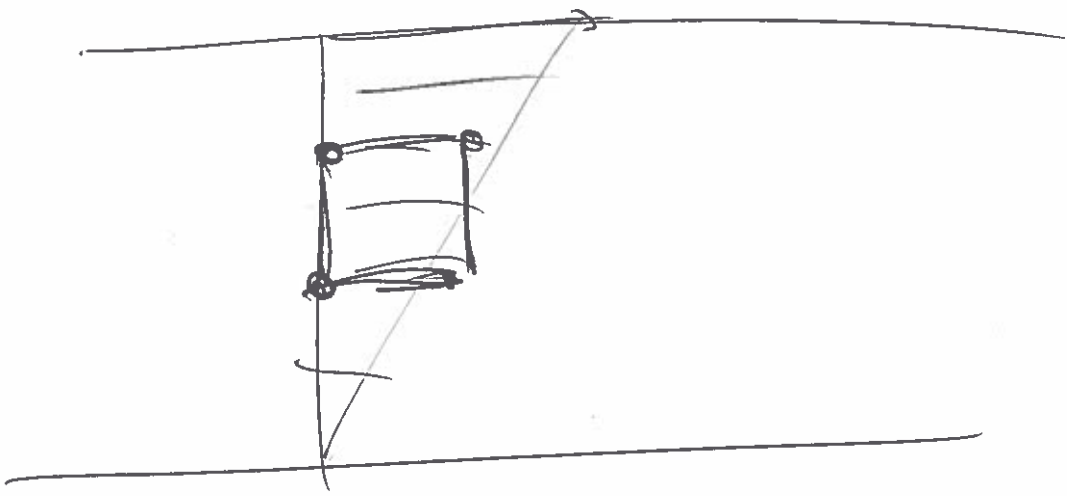
$$\begin{pmatrix} \frac{\partial u_1}{\partial x_1} & \frac{\partial u_1}{\partial x_2} \\ \frac{\partial u_2}{\partial x_1} & \frac{\partial u_2}{\partial x_2} \end{pmatrix} = \begin{pmatrix} 0 & u \\ 0 & 0 \end{pmatrix}$$

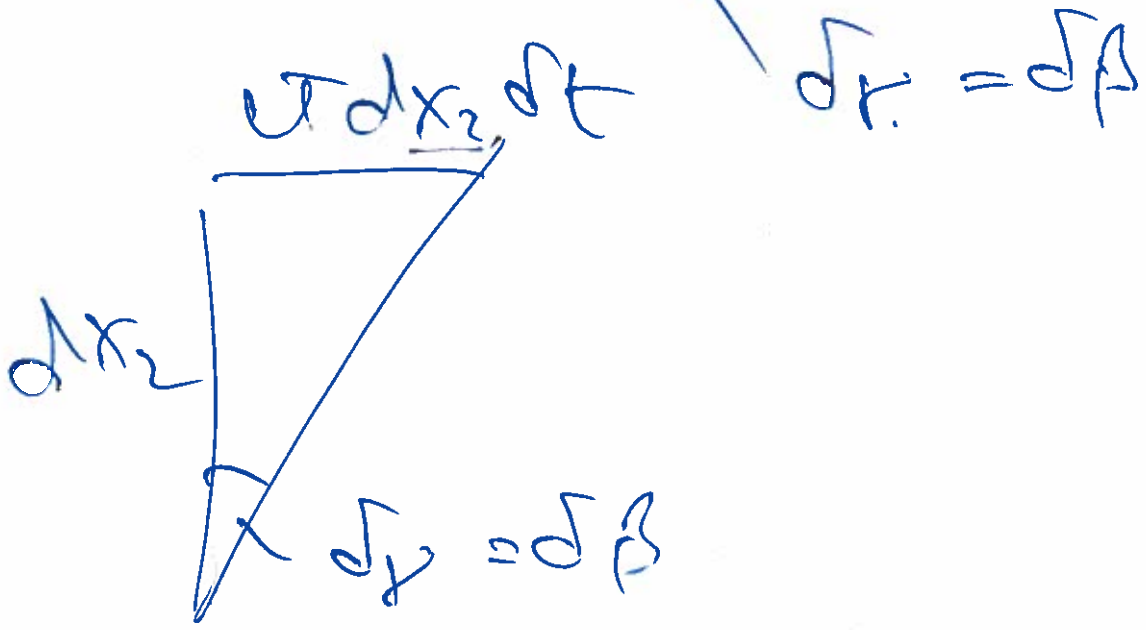
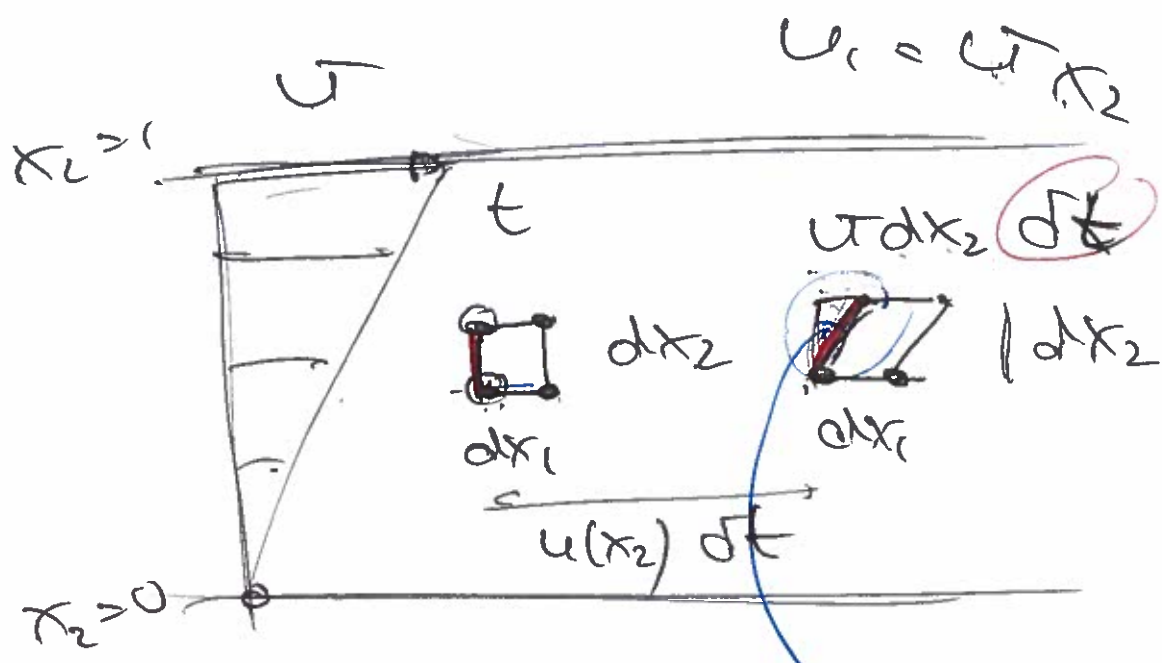
$$[\varepsilon_{ij}]$$



(2)

$$[\omega_{ij}] =$$



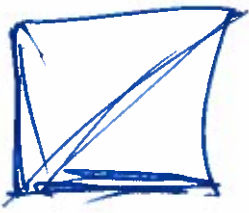


$$\underbrace{\int \delta \beta}_{\delta \beta} = \frac{u dx_2 dt}{dx_2}$$

$$\frac{\delta \beta}{dt} = u$$

Av. rate of rotation

(4)



$d\beta$



$$\text{av. rate of rotation} = \frac{1}{2} \left[\frac{2}{1} + \frac{2}{1} \right]$$