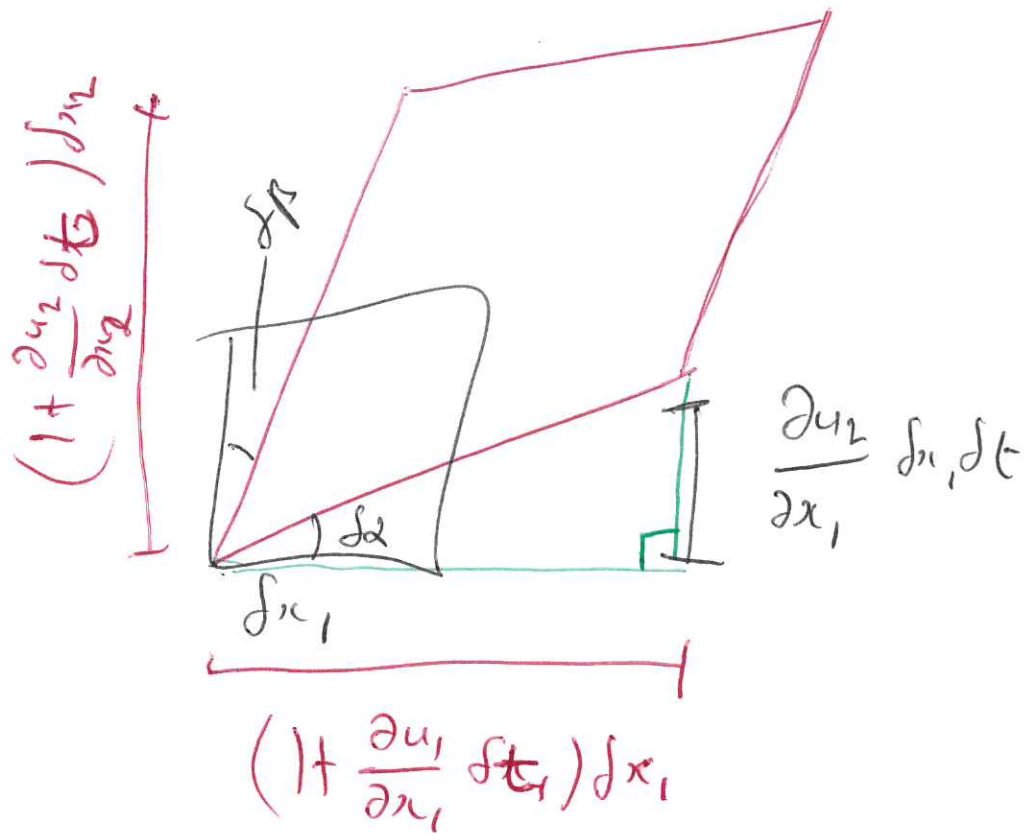


## (ii) Shear rate of strain



Change of shape of a small parcel of fluid body with rigid-body motion subtracted

$$\tan \alpha = \frac{\frac{\partial u_2}{\partial x_1} dx_1, dt}{\left(1 + \frac{\partial u_1}{\partial x_1} dt\right) dx_1}$$

Now as  $dt \rightarrow 0$  ;  $\alpha \rightarrow 0$

$$\text{So } \alpha \approx \frac{\partial u_2}{\partial x_1} dt \quad (\text{neglecting quadratic terms})$$

In the limit

$$\boxed{\frac{D\alpha}{Dt} = \frac{\partial u_2}{\partial x_1}}$$

(material line)

Similarly

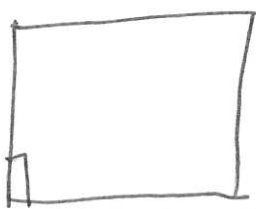
$$\frac{D\beta}{Dt} = \frac{\partial u_1}{\partial x_2}$$

(2)

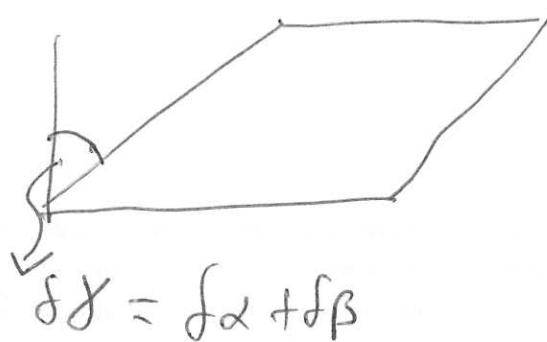
Now consider the "shear rate"

rate at which the right angle gets smaller

$t=0$



$\gamma=0$



(after rotation)

Thus

$$\frac{D\gamma}{Dt} = \frac{D\alpha}{Dt} + \frac{D\beta}{Dt} = \left( \frac{\partial u_2}{\partial x_1} + \frac{\partial u_1}{\partial x_2} \right) = 2 \epsilon_{12}$$

The off-diagonal entries in  $\epsilon_{ij}$  represent half the shear rate in a plane spanned by  $\underline{e}_i$  and  $\underline{e}_j$ .

Also

The change in angle of the main diagonal of the fluid rectangle is

$$\delta\phi = \frac{1}{2} (\delta\alpha - \delta\beta)$$

$$\begin{aligned} \text{So, } \frac{Dq}{Dt} &= \frac{1}{2} \left( \frac{D\alpha}{Dt} - \frac{D\beta}{Dt} \right) \\ &= \frac{1}{2} \left( \frac{\partial u_2}{\partial x_1} - \frac{\partial u_1}{\partial x_2} \right) = \omega_{21} = \omega_3 \end{aligned}$$

So rotation rate of main diagonal about  $\underline{e}_3$  is the vorticity, as shown earlier.

### Summary

Motion of fluid can be decomposed into

$$\underline{u}(\underline{x} + \underline{dx}) = \underbrace{\underline{u}(\underline{x})}_{\text{translation}} + \underbrace{\underline{\Omega} \times \underline{dx}}_{\text{rotation}} + \underbrace{\underline{E} \underline{dx}}_{\text{dilatation \& skew}}$$

rigid-body.

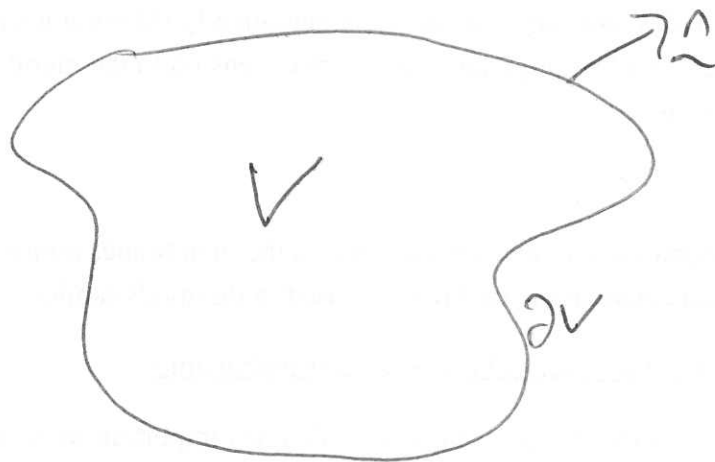
$$u_i(x_k + \delta x_k) = u_i(x_k) + \omega_{ij} \delta x_j + \epsilon_{ij} \delta x_j$$

# Equation of continuity

(4)

Physics: Mass flux into a spatially fixed control volume  
= rate of change of mass in that volume.

Integral form:



$$\text{Mass flux} = \text{density, } \rho \left[ \frac{\text{kg}}{\text{m}^3} \right] \times \text{velocity normal to} \left[ \frac{\text{m}}{\text{s}} \right] \\ \times \text{cross-sectional area} \left[ \text{m}^2 \right] = \left[ \frac{\text{kg}}{\text{s}} \right]$$

Rate of change of mass = total influx

$$\frac{d}{dt} \int_V \rho dV = \int -\rho \underline{u} \cdot \underline{n} dA$$

$\partial V \uparrow$  negative because

$\underline{n}$  is outer unit normal

[Volume is fixed  $\Rightarrow$  take  $\frac{\partial}{\partial t}$  inside]

$$\int_V \frac{\partial \rho}{\partial t} dV + \int_{\partial V} \rho \underline{u} \cdot \underline{n} dA = 0$$

(5)

Now use divergence theorem

$$\int_V \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \underline{u}) dV = 0$$

✓

This is true for every possible volume  $V$ ,

$$\text{So } \boxed{\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \underline{u}) = 0} \leftarrow \text{continuity equation}$$

In index notation

$$\frac{\partial (\rho u_i)}{\partial x_i} + \frac{\partial \rho}{\partial t} = 0$$

$$\Rightarrow \rho \frac{\partial u_i}{\partial x_i} + \underbrace{u_i \frac{\partial \rho}{\partial x_i}}_{\frac{D\rho}{Dt}} + \frac{\partial \rho}{\partial t} = 0$$

$$\Rightarrow \boxed{\frac{D\rho}{Dt} + \rho \frac{\partial u_i}{\partial x_i} = 0}$$

$$\frac{D\rho}{Dt}$$

is the rate of change of density of material fluid elements.

(6)

For an incompressible fluid,  $\frac{D\rho}{Dt} = 0$

& then

$$\left. \begin{aligned} \frac{\partial u_i}{\partial x_i} &= 0 \\ \text{i.e. } \operatorname{div} \underline{u} &= 0 \end{aligned} \right\}$$

This is "conservation of volume" and is a purely kinematic constraint!