

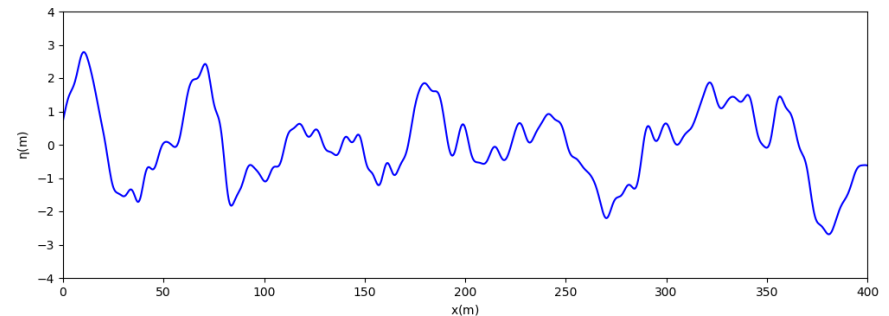
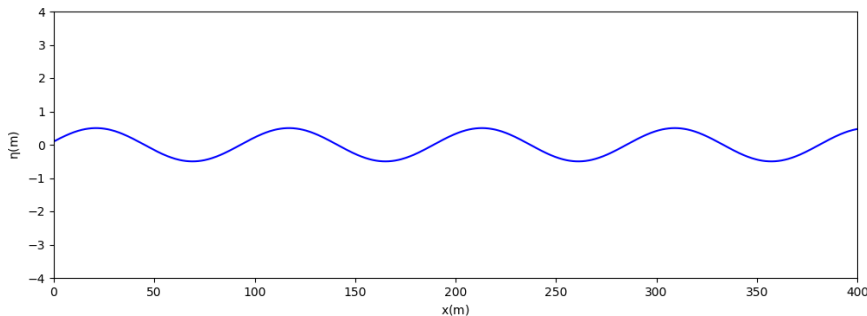
Waves

3. Statistics and Irregular Waves



Statistics and Irregular Waves

- Real wave fields are not regular
- Combination of many periods, heights, directions
- Design and simulation require realistic wave statistics:
 - **probability distribution** of heights
 - **energy spectrum** of frequencies (and directions)



Statistics and Irregular Waves

3. STATISTICS AND IRREGULAR WAVES

3.1 Measures of height and period

3.2 Probability distribution of wave heights

3.3 Wave spectra

3.4 Reconstructing a wave field

3.5 Prediction of wave climate



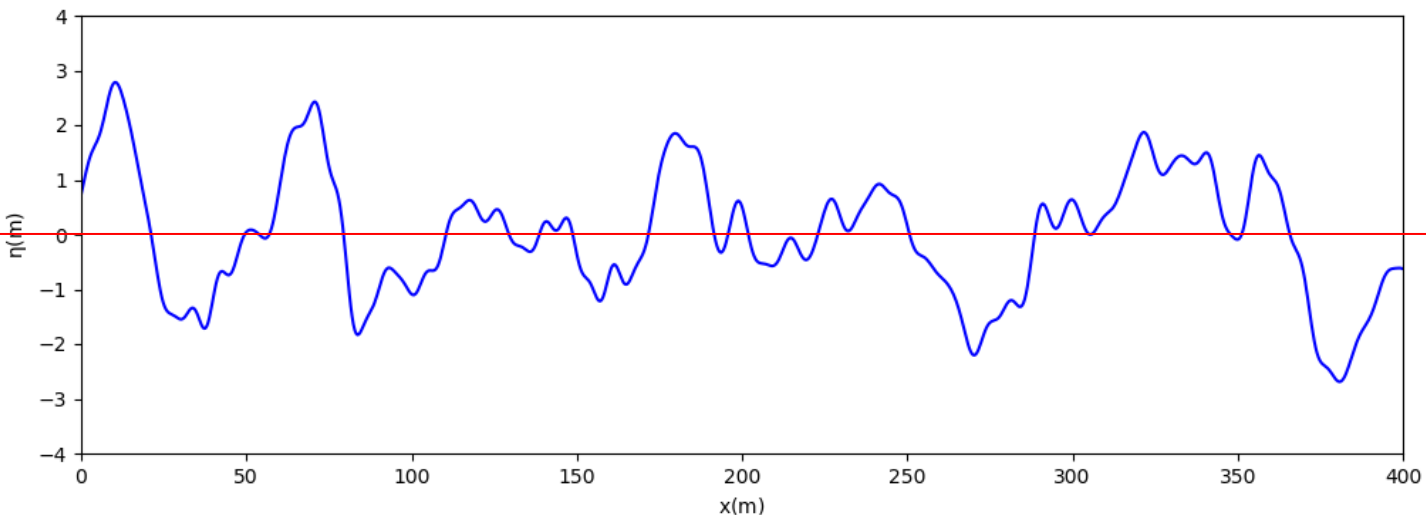
Measures of Wave Height

H_{\max}	Largest wave height in the sample	$H_{\max} = \max_i(H_i)$
H_{av}	Mean wave height	$H_{\text{av}} = \frac{1}{N} \sum H_i$
H_{rms}	Root-mean-square wave height	$H_{\text{rms}} = \sqrt{\frac{1}{N} \sum H_i^2}$
$H_{1/3}$	Average of the highest $N/3$ waves	$H_{1/3} = \frac{1}{N/3} \sum_1^{N/3} H_i$
H_{m0}	Estimate based on the rms surface elevation	$H_{m0} = 4(\overline{\eta^2})^{1/2}$
H_s	Significant wave height	Either $H_{1/3}$ or H_{m0}



Measures of Wave Period

T_s	Significant wave period (average of highest $N/3$ waves)
T_p	Peak period (from peak frequency of energy spectrum)
T_e	Energy period (period of a regular wave with same significant wave height and power density; used in wave-energy prediction; derived from energy spectrum)
T_z	Mean zero up-crossing period



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Probability Distribution of Wave Heights

For a narrow-banded frequency spectrum the **Rayleigh probability distribution** is appropriate:

$$P(\text{height} > H) = \exp\left[-(H/H_{\text{rms}})^2\right]$$

Cumulative distribution function:

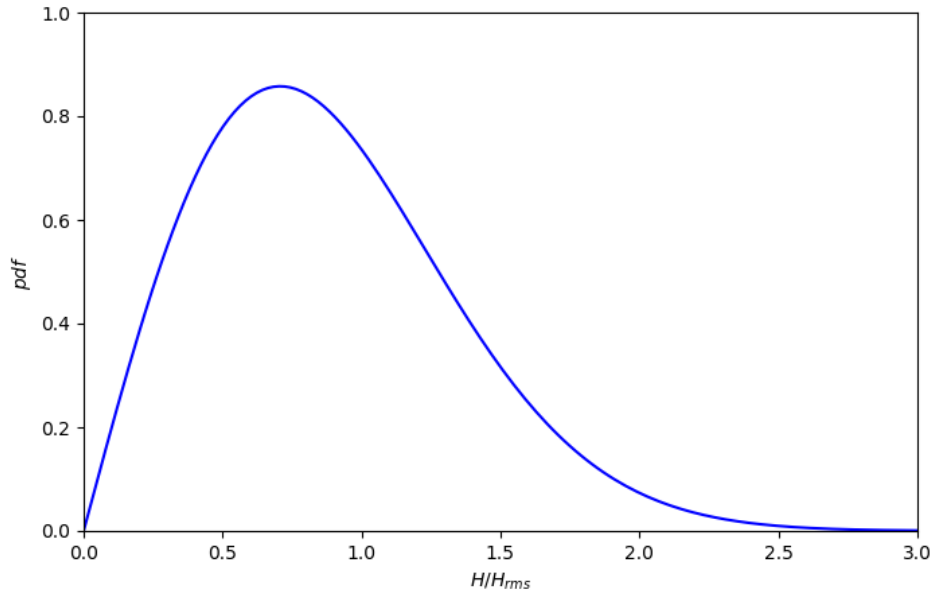
$$F(H) = P(\text{height} < H) = 1 - e^{-(H/H_{\text{rms}})^2}$$

Probability density function:

$$f(H) = \frac{dF}{dH} = 2 \frac{H}{H_{\text{rms}}^2} e^{-(H/H_{\text{rms}})^2}$$



Rayleigh Distribution



$$f(H) = 2 \frac{H}{H_{rms}^2} e^{-(H/H_{rms})^2}$$

Single parameter: H_{rms}

$$H_{rms}^2 \equiv E(H^2) = \int_0^{\infty} H^2 f(H) dH$$

$$H_{av} \equiv E(H) = \int_0^{\infty} H f(H) dH$$

$$H_{av} = \frac{\sqrt{\pi}}{2} H_{rms} = 0.886 H_{rms}$$

$$H_{1/3} = 1.416 H_{rms}$$

$$H_{1/10} = 1.800 H_{rms}$$

$$H_{1/100} = 2.359 H_{rms}$$



Example

Near a pier, 400 consecutive wave heights are measured. Assume that the sea state is narrow-banded.

- (a) How many waves are expected to exceed $2H_{\text{rms}}$?
- (b) If the significant wave height is 2.5 m, what is H_{rms} ?
- (c) Estimate the wave height exceeded by 80 waves.
- (d) Estimate the number of waves with a height between 1.0 m and 3.0 m.



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(a) $P(\text{height} > H) = e^{-(H/H_{\text{rms}})^2}$
 $P(\text{height} > 2H_{\text{rms}}) = e^{-4} = 0.01832$
In 400 waves, $n = 400 \times 0.01832 = \mathbf{7.328}$

(b) $H_{1/3} = 1.416 H_{\text{rms}}$
 $2.5 = 1.416 H_{\text{rms}}$
 $H_{\text{rms}} = \mathbf{1.766 \text{ m}}$

(c) $P(\text{height} > H) = e^{-(H/H_{\text{rms}})^2} = \frac{80}{400} = 0.2$
 $(H/H_{\text{rms}})^2 = -\ln 0.2$
 $H = H_{\text{rms}} \times \sqrt{-\ln 0.2} = \mathbf{2.240 \text{ m}}$

(d) $P(1.0 < \text{height} < 3.0) = P(\text{height} > 1.0) - P(\text{height} > 3.0)$
 $= e^{-(1.0/H_{\text{rms}})^2} - e^{-(3.0/H_{\text{rms}})^2}$
 $= 0.6699$
In 400 waves, $n = 400 \times 0.6699 = \mathbf{268.0}$



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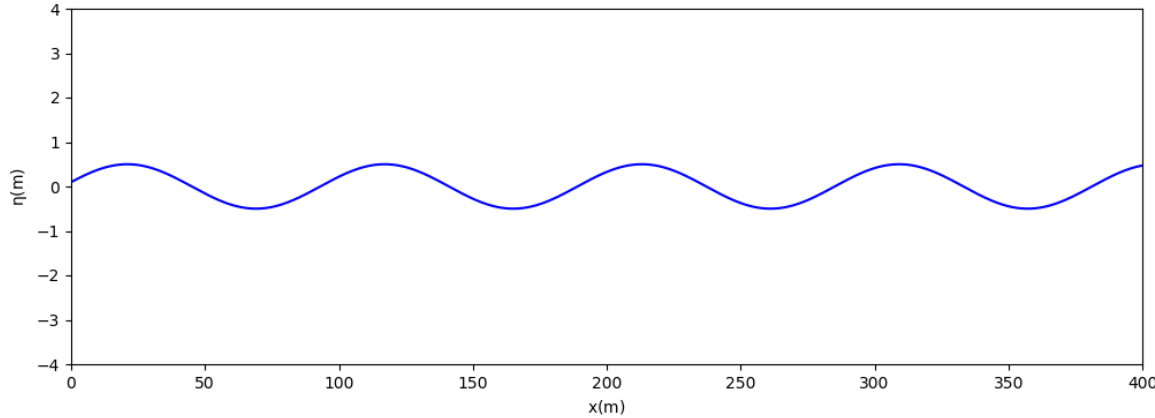
3.3 Wave spectra

3.4 Reconstructing a wave field

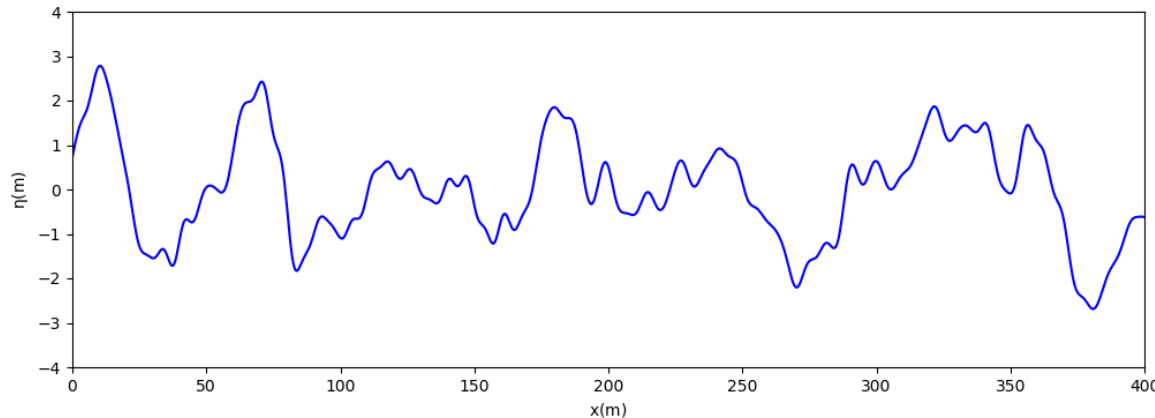
3.5 Prediction of wave climate



Regular vs Irregular Waves



Regular wave:
- single frequency



Irregular wave:
- many frequencies

Wave **energy** depends on $\overline{\eta^2}$



Energy Spectrum

- “**Spectral**” means “**by frequency**”
- A **spectrum** is usually determined by a **Fourier transform**
- This splits a signal up into its **component frequencies**

- **Energy** in a wave is proportional to $\overline{\eta^2}$, where η is surface displacement
- The **energy spectrum**, or **power spectrum**, is the Fourier transform of η^2



Energy Spectrum

For **regular** waves (single frequency):

$$\eta = A \cos(kx - \omega t)$$

$$E = \frac{1}{2} \rho g A^2 = \rho g \overline{\eta^2(t)} = \frac{1}{8} \rho g H^2$$

For **irregular** waves (many frequencies):

$S(f) df$ is the “energy” in a small interval df near frequency f

$\int_{f_1}^{f_2} S(f) df$ is the “energy” between frequencies f_1 and f_2

(strictly: energy/ ρg)

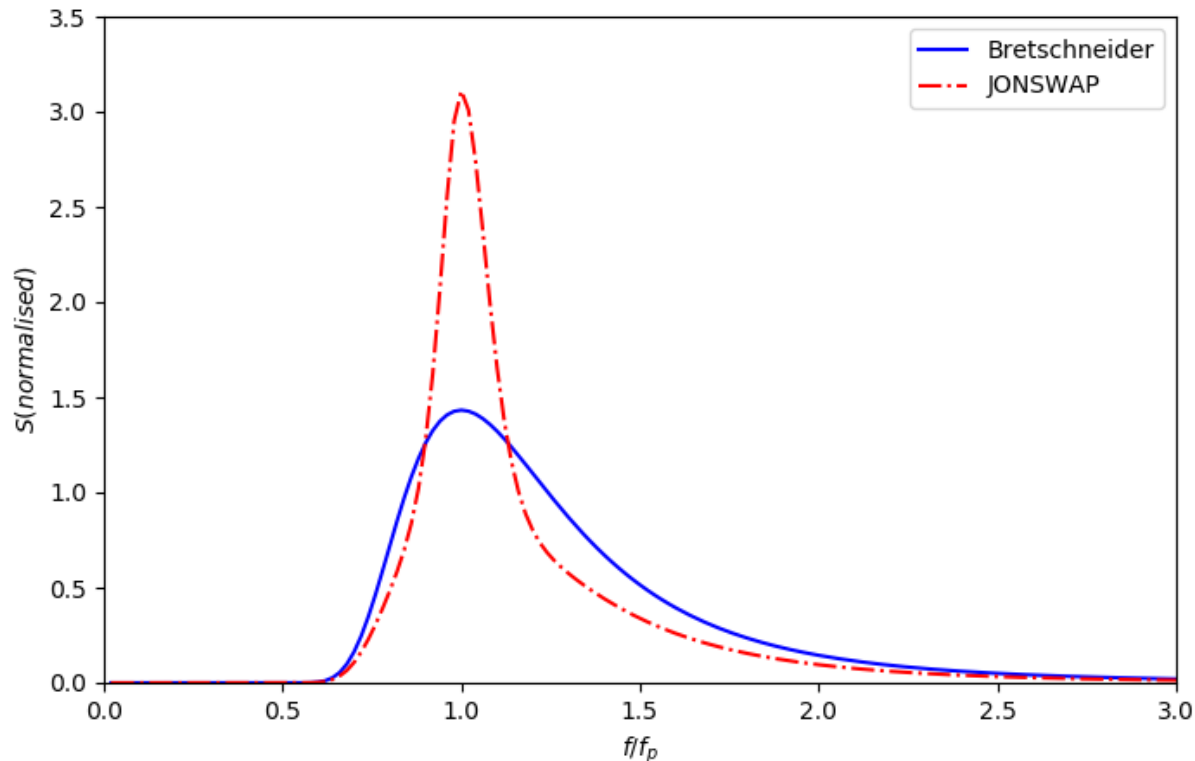
The **energy spectrum** $S(f)$ is determined by Fourier transforming η^2



Model Spectra

Open ocean: **Bretschneider spectrum**

Fetch-limited seas: **JONSWAP spectrum**



Key parameters: **peak frequency** f_p ($=1/(\text{peak period}, T_p)$)
significant wave height H_{m0}



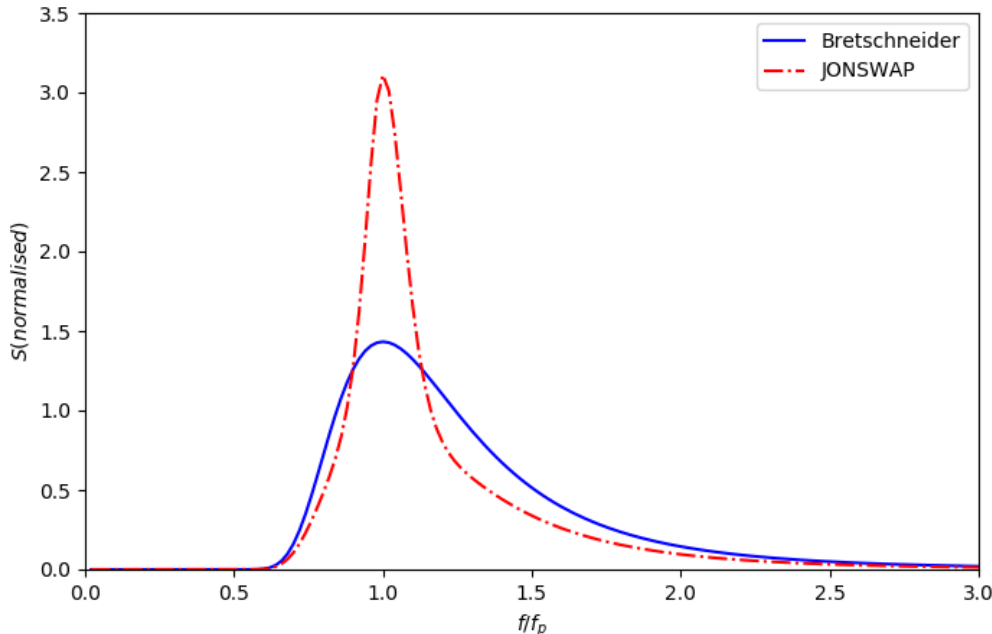
Model Spectra

Bretschneider spectrum:

$$S(f) = \frac{5}{16} H_{m0}^2 \frac{f_p^4}{f^5} \exp\left(-\frac{5}{4} \frac{f_p^4}{f^4}\right)$$

JONSWAP spectrum:

$$S(f) = C H_{m0}^2 \frac{f_p^4}{f^5} \exp\left(-\frac{5}{4} \frac{f_p^4}{f^4}\right) \gamma^b$$



$$b = \exp\left\{-\frac{1}{2} \left(\frac{f/f_p - 1}{\sigma}\right)^2\right\}$$

$$\sigma = \begin{cases} 0.07 & f < f_p \\ 0.09 & f > f_p \end{cases}$$

$$\gamma = 3.3$$



Significant Wave Height, H_{m0}

Bretschneider **spectrum**:

$$S(f) = \frac{5}{16} H_{m0}^2 \frac{f_p^4}{f^5} \exp\left(-\frac{5}{4} \frac{f_p^4}{f^4}\right)$$

Total energy:

$$\frac{E}{\rho g} \equiv \int_0^{\infty} S(f) df = \frac{1}{16} H_{m0}^2$$

$$H_{m0} = 4\sqrt{E/\rho g} = 4\sqrt{\eta^2(t)}$$

Total energy for a **regular wave**:

$$\frac{E}{\rho g} = \frac{1}{8} H_{rms}^2$$

Same energy if

$$H_{m0} = \sqrt{2} H_{rms} = 1.414 H_{rms}$$

Rayleigh distribution:

$$H_{1/3} = 1.416 H_{rms}$$

H_{m0} and $H_{1/3}$ can be used synonymously for H_s ...

... but H_{m0} is easier to measure!



Finding Wave Parameters From a Spectrum

- Surface displacement $\eta(t)$ is measured (e.g. wave buoy)
- $\eta^2(t)$ is Fourier-transformed to get energy spectrum $S(f)$
- Height and period parameters are deduced from the peak and the **moments** of the spectrum:

$$m_n = \int_0^{\infty} f^n S(f) df$$

Peak period:

$$T_p = \frac{1}{f_p}$$

Significant wave height:

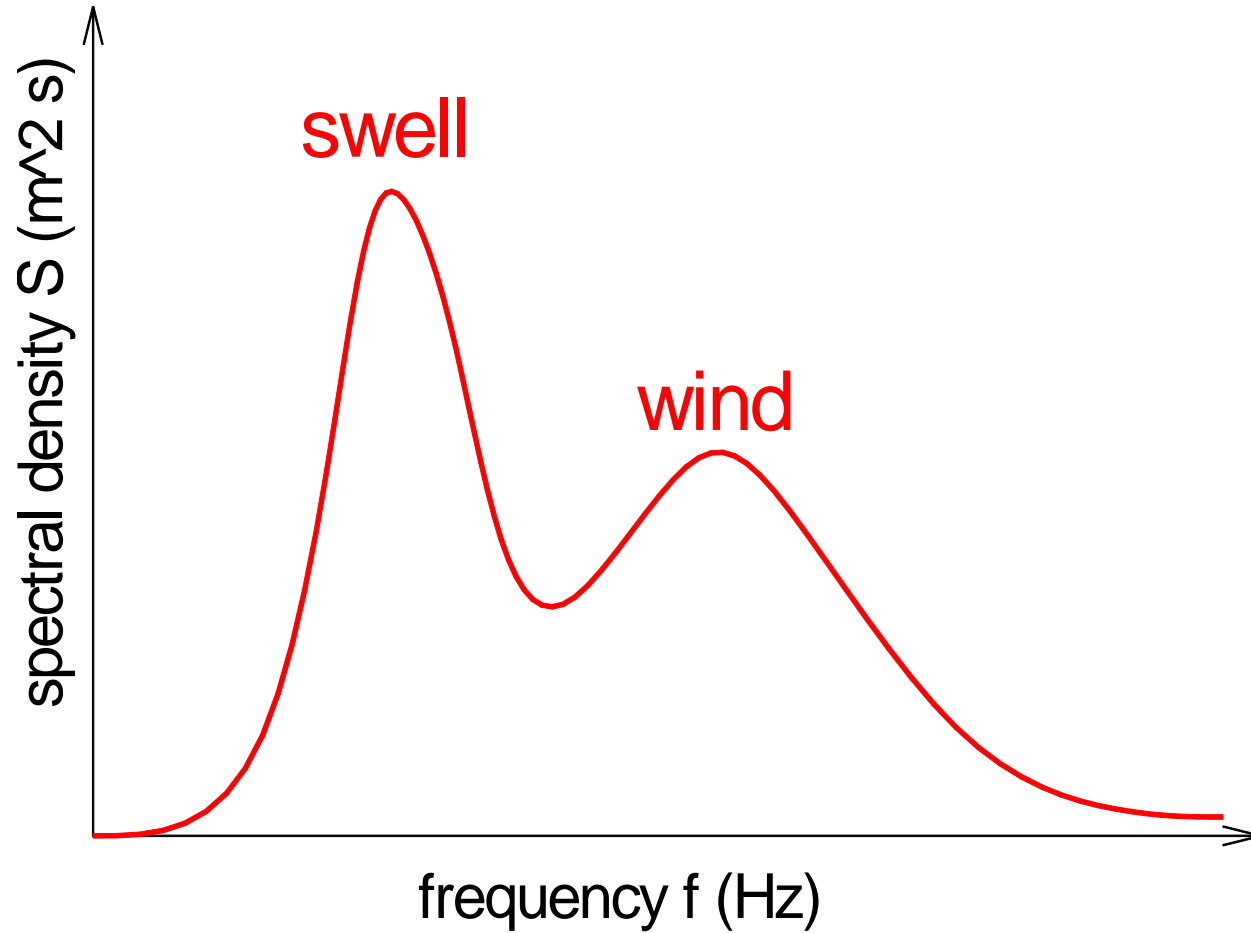
$$H_s = H_{m0} = 4\sqrt{m_0}$$

Energy period:

$$T_e = \frac{m_{-1}}{m_0}$$



Multi-Modal Spectra



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Using a Spectrum To Generate a Wave Field

$$\eta(t) = \sum a_i \cos(k_i x - \omega_i t - \phi_i)$$

amplitude

$$S(f_i)\Delta f = E_i = \frac{1}{2} a_i^2$$

$$a_i = \sqrt{2S(f_i)\Delta f}$$

(angular) frequency

$$\omega_i = 2\pi f_i$$

wavenumber

$$\omega_i^2 = g k_i \tanh k_i h$$

random phase



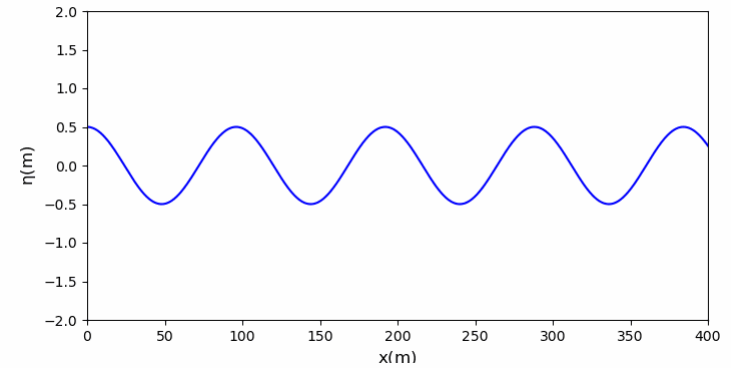
Simulated Wave Field

$$T_p = 8 \text{ s}$$

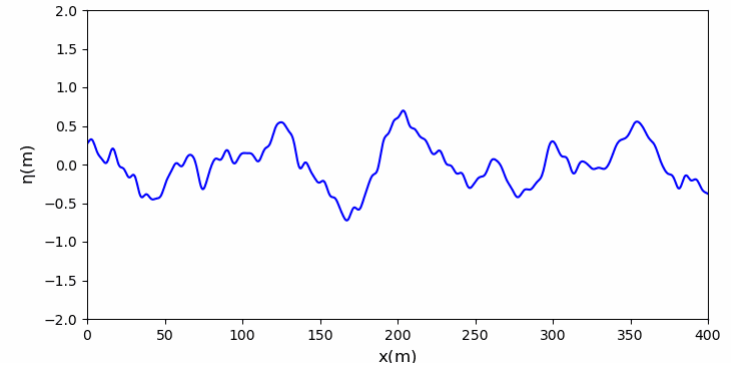
$$H_s = 1.0 \text{ m}$$

$$h = 30 \text{ m}$$

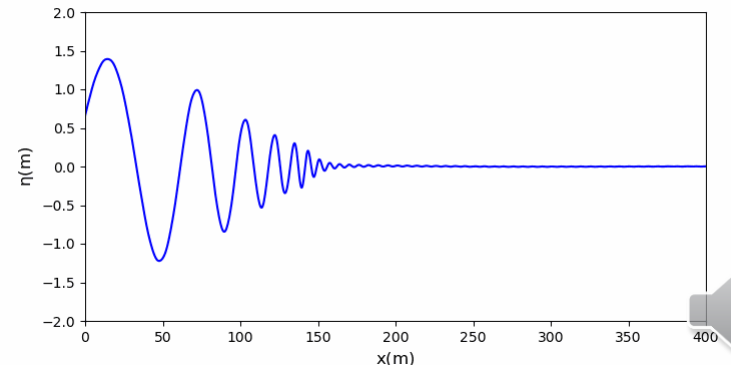
Regular waves:



Irregular waves:



Focused waves:



Example

An irregular wavefield at a deep-water location is characterised by peak period of 8.7 s and significant wave height of 1.5 m.

- (a) Provide a sketch of a Bretschneider spectrum, labelling both axes with variables and units and indicating the frequencies corresponding to both the peak period and the energy period.

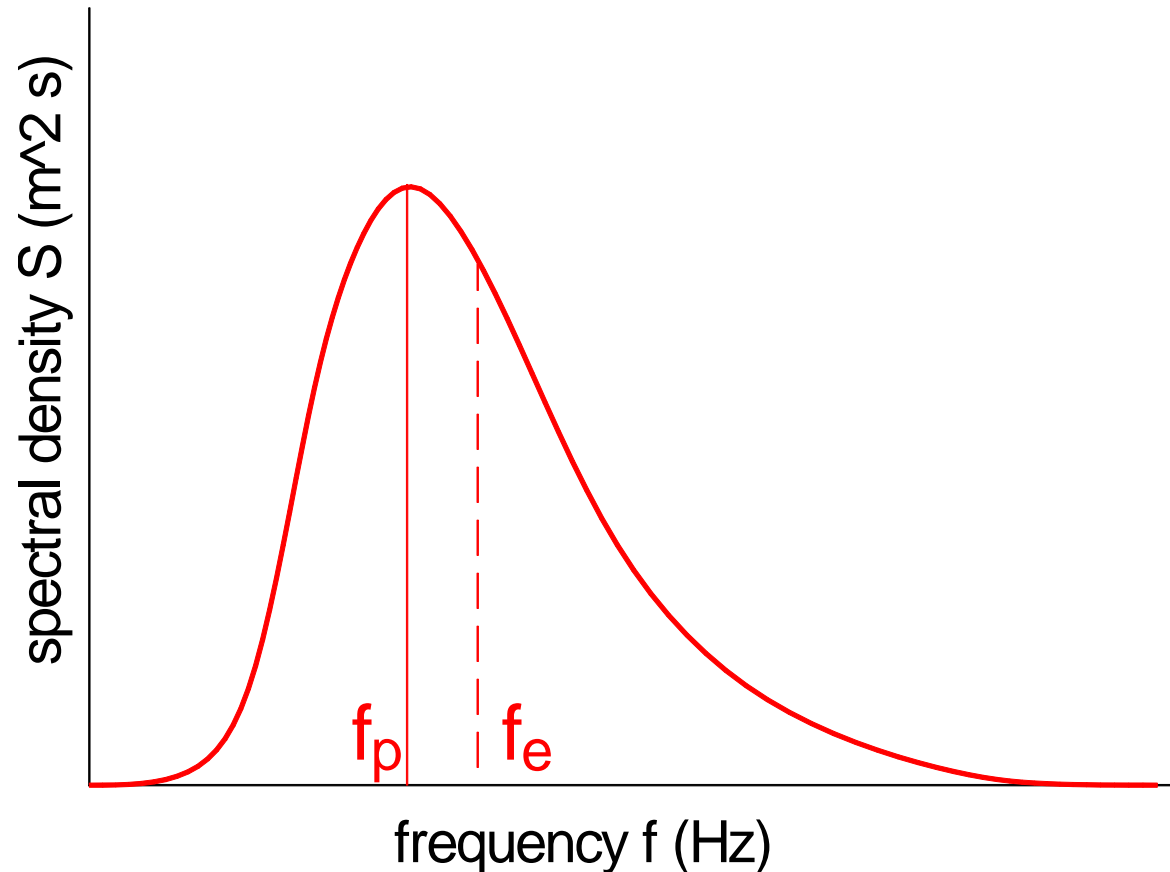
Note: Calculations are not needed for this part.

- (b) Determine the power density (in kW m^{-1}) of a regular wave component with frequency 0.125 Hz that represents the frequency range 0.12 to 0.13 Hz of the irregular wave field.



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An irregular wavefield at a deep-water location is characterised by peak period of 8.7 s and significant wave height of 1.5 m.

(b) Determine the power density (in kW m⁻¹) of a regular wave component with frequency 0.125 Hz that represents the frequency range 0.12 to 0.13 Hz of the irregular wave field.

$$T_p = 8.7 \text{ s} \quad H_s = 1.5 \text{ m}$$

$$f_p = \frac{1}{T_p} = 0.1149 \text{ Hz}$$

$$S(f) = \frac{5}{16} H_s^2 \frac{f_p^4}{f^5} \exp\left(-\frac{5}{4} \frac{f_p^4}{f^4}\right)$$

$$f = 0.125 \text{ Hz} \quad S(f) = 1.645 \text{ m}^2 \text{ s}$$

$$\Delta f = 0.01 \text{ Hz}$$

$$E = \rho g \times S(f) \Delta f = 165.4 \text{ J m}^{-2}$$

$$P = E c_g = E(nc)$$

$$\text{Deep water: } n = \frac{1}{2}$$

$$T = \frac{1}{f} = 8 \text{ s}$$

$$c = \frac{gT}{2\pi} = 12.49 \text{ m s}^{-1}$$

$$P = 1.033 \text{ kW m}^{-1}$$



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Terminology

A **wave climate** or **sea state** is a model wave spectrum, usually defined by a representative **height** and **period**, for use in:

- **forecasting** (from a weather forecast in advance)
- **nowcasting** (from ongoing weather)
- **hindcasting** (reconstruction from previous event)



Prediction of Sea State

Require: significant wave height, H_s
 significant wave period, T_s (or peak period, T_p)

Depend on: wind speed, U
 fetch, F
 duration, t
 gravity, g

Dimensional analysis:

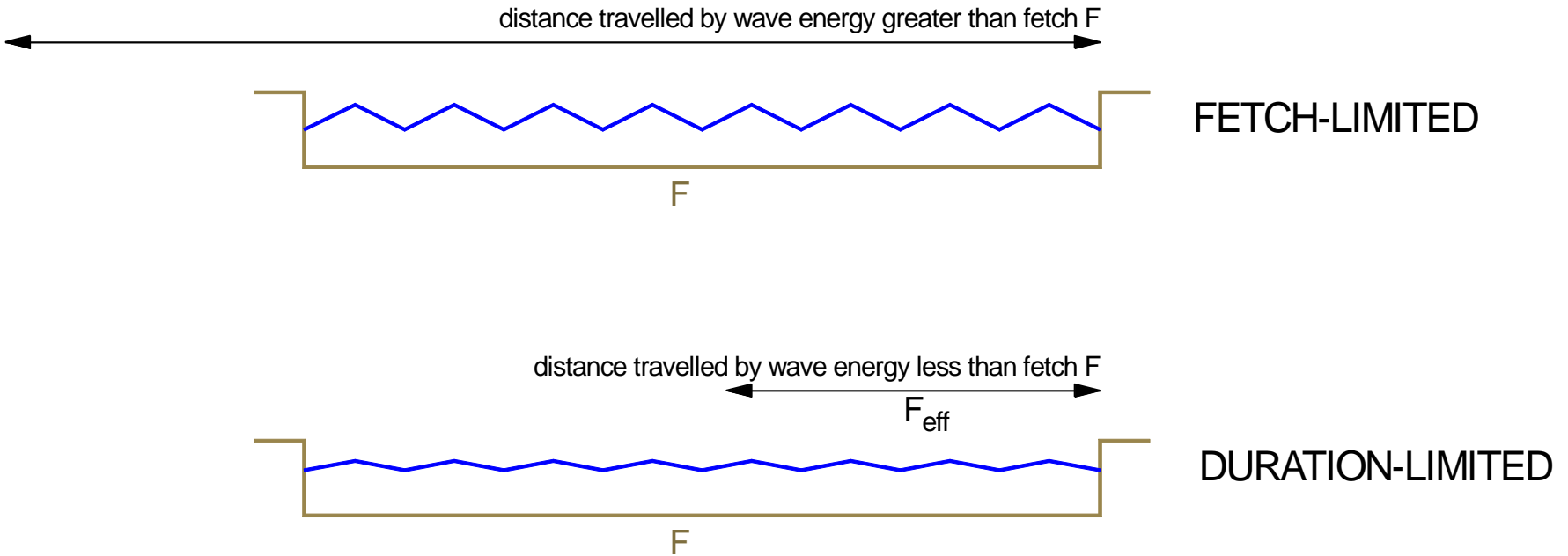
$$\frac{gH_s}{U^2} = \text{function}\left(\frac{gF}{U^2}, \frac{gt}{U}\right)$$

$$\frac{gT_p}{U} = \text{function}\left(\frac{gF}{U^2}, \frac{gt}{U}\right)$$

Empirical functions: **JONSWAP** or **SMB** curves



Fetch-Limited vs Duration-Limited



JONSWAP Curves

For **fetch-limited** waves:

$$\frac{gH_s}{U^2} = 0.0016 \left(\frac{gF}{U^2} \right)^{1/2} \quad (\text{up to maximum } 0.2433)$$

$$\frac{gT_p}{U} = 0.286 \left(\frac{gF}{U^2} \right)^{1/3} \quad (\text{up to maximum } 8.134)$$

Waves are fetch-limited provided the storm has blown for a minimum time t_{min} given by

$$\left(\frac{gt}{U} \right)_{\min} = 68.8 \left(\frac{gF}{U^2} \right)^{2/3} \quad (\text{up to maximum } 7.15 \times 10^4)$$

Otherwise the waves are **duration-limited**, and the fetch used to determine height and period is an effective fetch determined by inversion using the actual storm duration t :

$$\left(\frac{gF}{U^2} \right)_{\text{eff}} = \left(\frac{1}{68.8} \frac{gt}{U} \right)^{3/2}$$



JONSWAP Curves (reprise)

$$\hat{H}_s = 0.0016\hat{F}^{1/2}$$

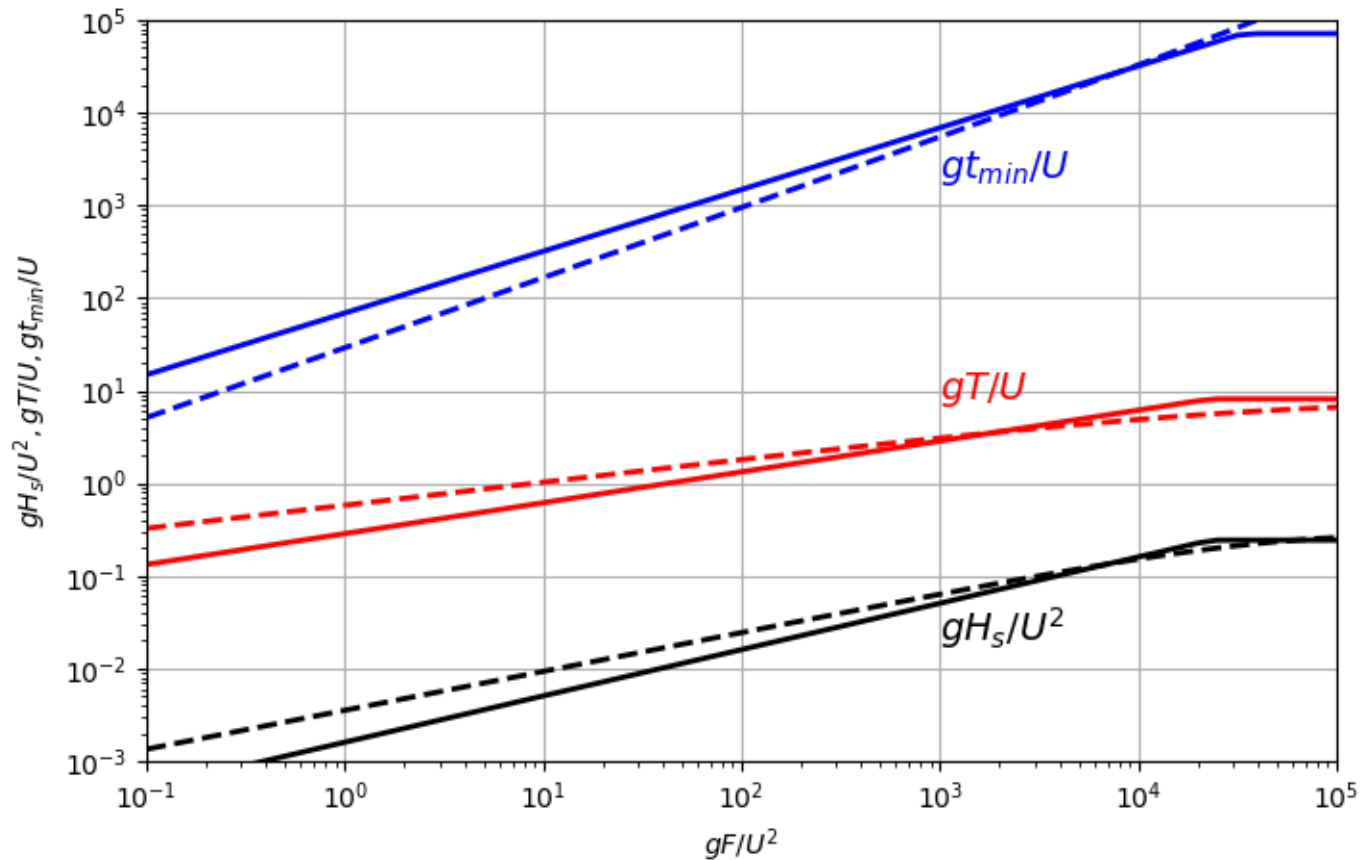
$$\hat{T}_p = 0.286\hat{F}^{1/3}$$

$$\hat{t}_{\min} = 68.8\hat{F}^{2/3}$$

$$\hat{F} \equiv \frac{gF}{U^2}, \quad \hat{t} \equiv \frac{gt}{U}, \quad \hat{H}_s \equiv \frac{gH_s}{U^2}, \quad \hat{T}_p \equiv \frac{gT_p}{U}$$



JONSWAP and SMB Curves



Solid lines: JONSWAP

Dashed lines: SMB



Example

- (a) Wind has blown at a consistent $U = 20 \text{ m s}^{-1}$ over a fetch $F = 100 \text{ km}$ for $t = 6 \text{ hrs}$. Determine H_s and T_p using the JONSWAP curves.
- (b) If the wind blows steadily for another 4 hours what are H_s and T_p ?



- (a) Wind has blown at a consistent $U = 20 \text{ m s}^{-1}$ over a fetch $F = 100 \text{ km}$ for $t = 6 \text{ hrs}$. Determine H_s and T_p using the JONSWAP curves.

$$U = 20 \text{ m s}^{-1}$$

$$F = 10^5 \text{ m}$$

$$t = 6 \times 3600 = 21600 \text{ s}$$

$$\hat{F} \equiv \frac{gF}{U^2} = 2453$$

$$\hat{t} \equiv \frac{gt}{U} = 10590 \quad \hat{t}_{\min} = 68.8\hat{F}^{2/3} = 12510$$

Duration-limited

$$\hat{F}_{\text{eff}} = \left(\frac{\hat{t}}{68.8} \right)^{3/2} = 1910$$

$$\hat{H}_s = 0.0016\hat{F}_{\text{eff}}^{1/2} = 0.06993$$

$$\hat{T}_p = 0.286\hat{F}_{\text{eff}}^{1/3} = 3.548$$

$$H_s = \hat{H}_s \times \frac{U^2}{g} = \mathbf{2.851 \text{ m}}$$

$$T_p = \hat{T}_p \times \frac{U}{g} = \mathbf{7.233 \text{ s}}$$

$$\hat{H}_s = 0.0016\hat{F}^{1/2}$$

$$\hat{T}_p = 0.286\hat{F}^{1/3}$$

$$\hat{t}_{\min} = 68.8\hat{F}^{2/3}$$

$$\hat{F} \equiv \frac{gF}{U^2} \quad \hat{H}_s \equiv \frac{gH_s}{U^2} \quad \hat{t} \equiv \frac{gt}{U}$$



(b) If the wind blows steadily for another 4 hours what are H_s and T_p ?

$$U = 20 \text{ m s}^{-1}$$

$$F = 10^5 \text{ m}$$

$$\hat{F} = 2453$$

$$\hat{t}_{\min} = 12510$$

$$t = 10 \times 3600 = 36000 \text{ s}$$

$$\hat{t} = \frac{gt}{U} = 17660 \quad \text{Fetch-limited}$$

$$\hat{H}_s = 0.0016\hat{F}^{1/2} = 0.07924$$

$$H_s = \hat{H}_s \times \frac{U^2}{g} = \mathbf{3.231 \text{ m}}$$

$$\hat{T}_p = 0.286\hat{F}^{1/3} = 3.857$$

$$T_p = \hat{T}_p \times \frac{U}{g} = \mathbf{7.863 \text{ s}}$$

$$\hat{H}_s = 0.0016\hat{F}^{1/2}$$

$$\hat{T}_p = 0.286\hat{F}^{1/3}$$

$$\hat{t}_{\min} = 68.8\hat{F}^{2/3}$$

$$\hat{F} \equiv \frac{gF}{U^2} \quad \hat{H}_s \equiv \frac{gH_s}{U^2} \quad \hat{t} \equiv \frac{gt}{U}$$

