

Waves

4. Wave Loading On Structures



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4. WAVE LOADING ON STRUCTURES

4.1 Pressure distribution

4.2 Surface-piercing structure

4.3 Fully-submerged structure

4.4 Loads on a vertical (caisson-type) breakwater



Wave Pressure Forces

Pressure force: sum of (pressure x area) $\int p \, dA$

per unit width: $\int p \, dz$

Pressure distribution (progressive wave):

$$p = \underbrace{-\rho g z}_{\text{hydrostatic}} - \underbrace{\rho \frac{\partial \phi}{\partial t}}_{\text{wave}} = -\rho g z + \rho g A \frac{\cosh k(h+z)}{\cosh kh} \cos(kx - \omega t)$$

Wave component of pressure, with **reflection** (standing wave):

$$p = 2\rho g A \frac{\cosh k(h+z)}{\cosh kh} \cos kx \cos \omega t$$



Wave Pressure Forces

Maximum pressure at the structure:

$$p = \rho g H \frac{\cosh k(h+z)}{\cosh kh}$$

- $H (= 2A)$ is the **height of the incident wave**
- With reflection, $\eta_{\max} = 2A = H$ is also the **maximum crest height** above SWL.



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Surface-Piercing Structure

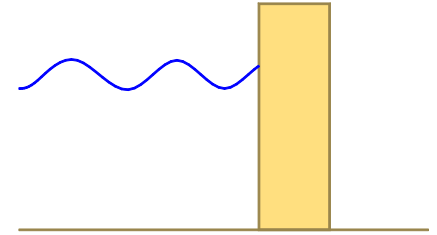
$$p = \rho g H \frac{\cosh k(h+z)}{\cosh kh}$$

$$F = \int p \, dz = \frac{\rho g H}{\cosh kh} \int_{z=-h}^0 \cosh k(h+z) \, dz$$

$$= \frac{\rho g H}{\cosh kh} \left[\frac{\sinh k(h+z)}{k} \right]_{-h}^0$$

$$= \frac{\rho g H \sinh kh}{k \cosh kh}$$

$$F = \frac{\rho g H \tanh kh}{k}$$



Shallow water: $F = \rho g H h$ (hydrostatic)

Deep water: $F = \frac{\rho g H}{k}$ (independent of depth)



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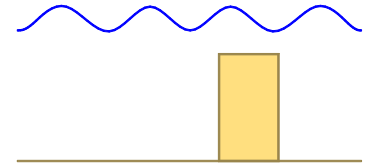
4.3 Fully-submerged structure

4.4 Loads on a vertical (caisson-type) breakwater



Fully-Submerged Structure

$$F = \int p \, dz = \frac{\rho g H}{\cosh kh} \int_{z=-h}^{-(h-B)} \cosh k(h+z) \, dz$$



$$F = \frac{\rho g H \sinh kB}{k \cosh kh}$$

This is always less than the surface-piercing case



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Breakwater Types

- Rubble-mound
- Caisson
- Floating



Rubble-Mound Breakwater



Caisson Breakwater



Floating Breakwater



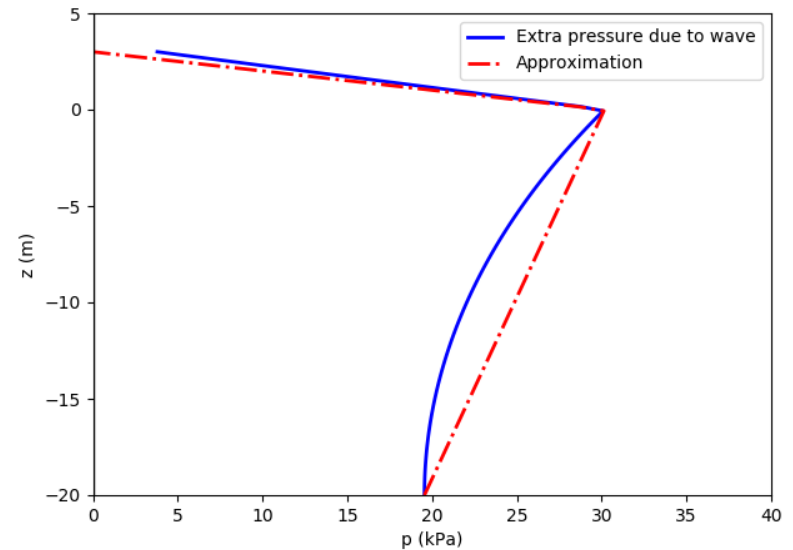
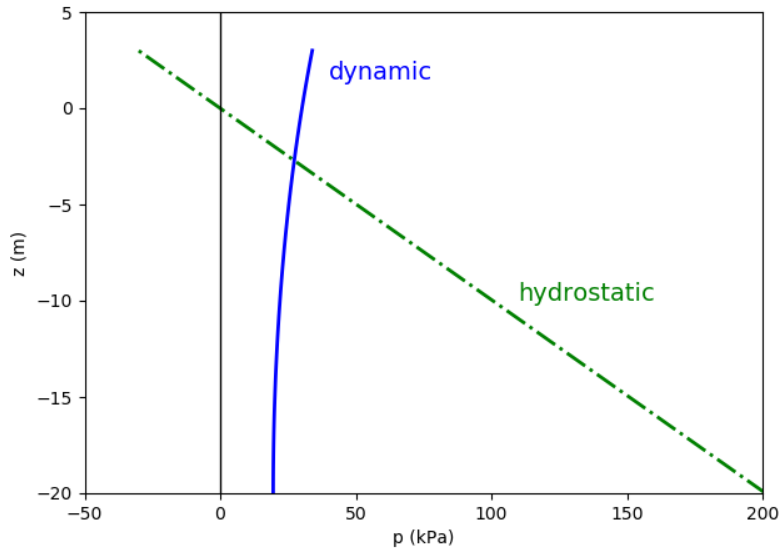
MULBERRY HARBOURS
The Mulberry Harbours were temporary harbours built by the Allies during the Second World War to support the invasion of Normandy.

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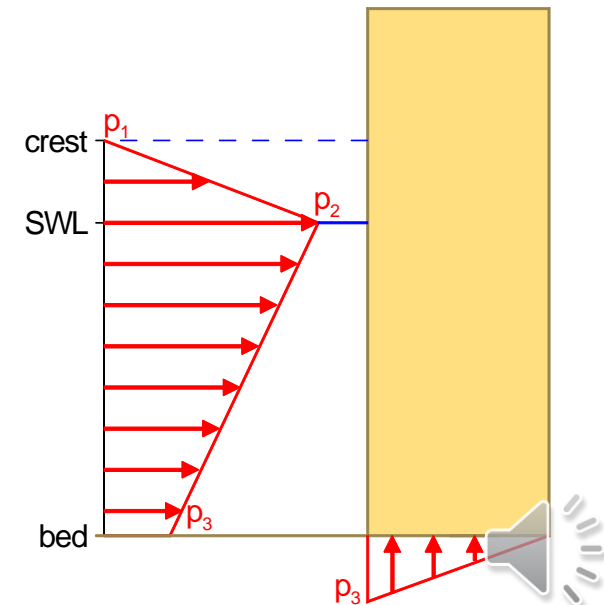
Wave Loading: Design Approximation



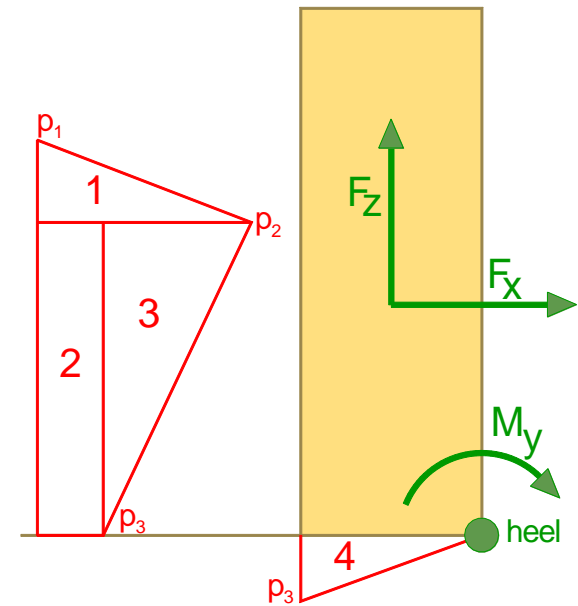
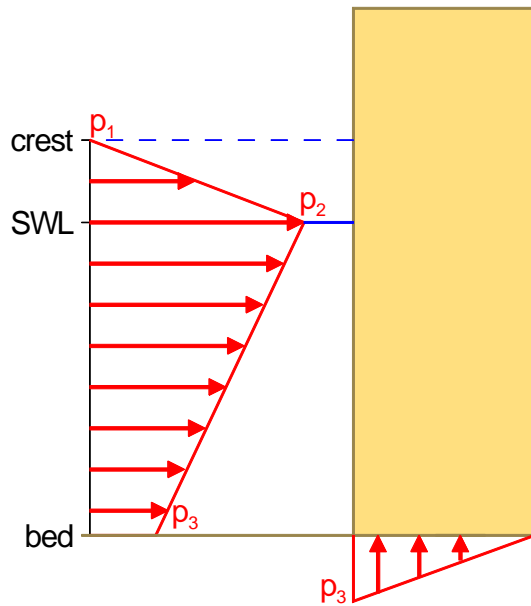
$$= \underbrace{-\rho g z}_{\text{hydrostatic}} + \underbrace{\rho g H \frac{\cosh k(h+z)}{\cosh kh}}_{\text{wave}}$$

Approximation for excess pressure:

- **hydrostatic** from wave crest down to SWL;
- **linear** between SWL and bed.



Wave Loading: Design Approximation



$$p_1 = 0$$

$$p_2 = \rho g H$$

$$p_3 = \frac{\rho g H}{\cosh kh}$$

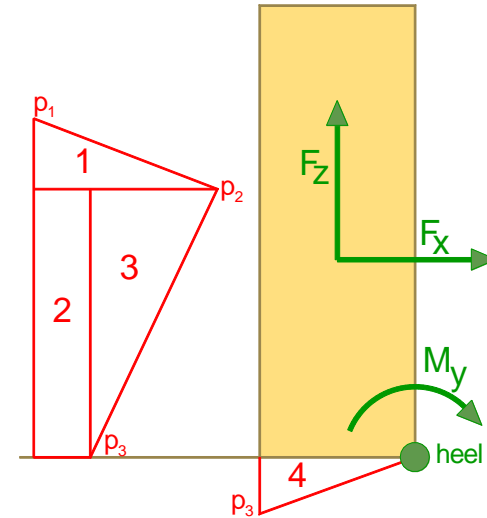


Wave Loading: Design Approximation

$$p_1 = 0$$

$$p_2 = \rho g H$$

$$p_3 = \frac{\rho g H}{\cosh kh}$$



Force	moment arm
$F_{1x} = \frac{1}{2} p_2 H$	$z_1 = h + \frac{1}{3} H$
$F_{2x} = p_3 h$	$z_2 = \frac{1}{2} h$
$F_{3x} = \frac{1}{2} (p_2 - p_3) h$	$z_3 = \frac{2}{3} h$
$F_{4z} = \frac{1}{2} p_3 b$	$x_4 = \frac{2}{3} b$

Horizontal **force** (per unit width):

$$F_x = F_{1x} + F_{2x} + F_{3x}$$

Overtuning **moment** (per unit width):

$$M = F_{1x} z_1 + F_{2x} z_2 + F_{3x} z_3 (+F_{4z} x_4)$$



Example

A regular wave of period 8 s and height 1.2 m is normally incident to a caisson-type breakwater of 4 m breadth and located in water depth of 5 m. Using linear theory, determine the following:

- (a) Caisson height required for 1 m freeboard above the peak wave elevation at the breakwater.
- (b) Maximum wave-induced horizontal force per metre of wave crest.
- (c) Maximum wave-induced overturning moment per metre of wave crest.



A regular wave of period 8 s and height 1.2 m is normally incident to a caisson-type breakwater of 4 m breadth and located in water depth of 5 m. Using linear theory, determine the following:

- (a) Caisson height required for 1 m freeboard above the peak wave elevation at the breakwater.

Approach wave amplitude: $A = H/2$ $H = 1.2 \text{ m}$

With reflection: $2A = H$

Add water depth (5 m) and freeboard (1 m):

$$\text{caisson height} = 5 + 1.2 + 1 = 7.2 \text{ m}$$



A regular wave of period 8 s and height 1.2 m is normally incident to a caisson-type breakwater of 4 m breadth and located in water depth of 5 m. Using linear theory, determine the following:

- (b) Maximum wave-induced horizontal force per metre of wave crest.
- (c) Maximum wave-induced overturning moment per metre of wave crest.

$$h = 5 \text{ m}$$

$$T = 8 \text{ s}$$

$$\omega = \frac{2\pi}{T} = 0.7854 \text{ rad s}^{-1}$$

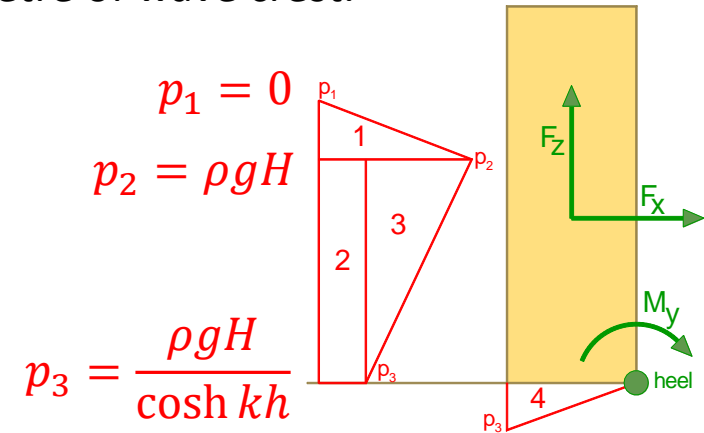
$$\omega^2 = gk \tanh kh$$

$$\frac{\omega^2 h}{g} = kh \tanh kh$$

$$0.3144 = kh \tanh kh$$

$$kh = \frac{0.3144}{\tanh kh} \quad \text{or} \quad kh = \frac{1}{2} \left(kh + \frac{0.3144}{\tanh kh} \right)$$

$$kh = 0.5918$$



A regular wave of period 8 s and height 1.2 m is normally incident to a caisson-type breakwater of 4 m breadth and located in water depth of 5 m. Using linear theory, determine the following:

(b) Maximum wave-induced horizontal force per metre of wave crest.

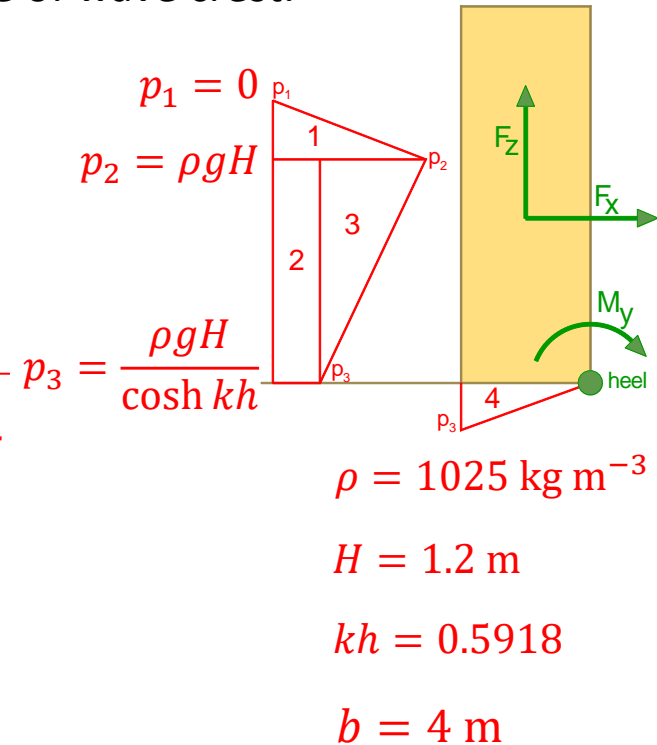
(c) Maximum wave-induced overturning moment per metre of wave crest.

$$p_1 = 0$$

$$p_2 = 12070 \text{ Pa}$$

$$p_3 = 10220 \text{ Pa}$$

Region	Force per metre (N/m)	Moment arm (m)
1	$F_{x1} = \frac{1}{2} p_2 \times H = 7242$	$z_1 = h + \frac{1}{3} H = 5.4$
2	$F_{x2} = p_3 \times h = 51100$	$z_2 = \frac{1}{2} h = 2.5$
3	$F_{x3} = \frac{1}{2} (p_2 - p_3) \times h = 4625$	$z_3 = \frac{2}{3} h = 3.333$
4	$F_{z4} = \frac{1}{2} p_3 \times b = 20440$	$x_4 = \frac{2}{3} b = 2.667$



Horizontal force: $F_{x1} + F_{x2} + F_{x3} = 62970 \text{ N/m}$

Turning moment: $F_{x1}z_1 + F_{x2}z_2 + F_{x3}z_3 + F_{z4}x_4 = 236800 \text{ N m/m}$

