

Three hours

A formula sheet is provided at the end of the examination

**THE UNIVERSITY OF MANCHESTER**

**CONTINUUM MECHANICS**

**21 January 2020**

**09:45 – 12:45**

Answer **ALL SIX** questions.

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University approved calculators may be used.

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1. Show that the derivative

$$\overset{\circ}{\mathbf{A}} = \frac{\partial \mathbf{A}}{\partial t} - \mathbf{W}\mathbf{A}$$

of a vector  $\mathbf{A}$  is objective, where  $\mathbf{W}$  is the spin tensor. You may use the fact that  $\dot{\mathbf{F}} = \mathbf{L}\mathbf{F}$  without proof, where  $\mathbf{F}$  is the deformation gradient tensor and  $\mathbf{L}$  is the Eulerian velocity gradient tensor. Both  $\mathbf{L}$  and  $\mathbf{F}$  are defined on the formula sheet at the end of the examination.

[5 marks]

2. A mixture of two chemicals is transported within a continuum. The concentrations (masses per unit deformed volume) of the two chemicals  $a$  and  $b$  are given by  $A(\mathbf{R}, t)$  and  $B(\mathbf{R}, t)$ , respectively. The chemicals react in such a way that a mass of  $a$  is produced at a rate  $R_A$  per unit deformed volume and a mass of  $b$  is produced at a rate  $R_B$  per unit deformed volume.

(i) By starting from conservation of mass equations within a material volume, find two partial differential equations that describe the conservation of mass of each chemical.

[5 marks]

(ii) Assuming that there are no other sources or sinks of mass and that the total mass of both chemicals is conserved, find a relationship between  $R_A$  and  $R_B$ .

[3 marks]

(iii) Assume further that  $B$  evaporates from the surface of the continuum with constant mass-loss rate  $E$  per unit deformed area and that  $R_B$  is also a constant. Find the relationship between  $R_B$  and  $E$  which ensures that the mass of  $A$  does not change.

[2 marks]

3. A solid material is reinforced by a family of fibres, whose initial direction is described by the vector field  $\mathbf{a}(\mathbf{r})$ , where  $|\mathbf{a}| = 1$ .

(i) Show that fibres in a deformed configuration, described by a position vector  $\mathbf{R}$ , are given by  $\mathbf{A} = \mathbf{F}\mathbf{a}$ , where  $\mathbf{F} = \nabla_{\mathbf{r}}\mathbf{R}$  is the deformation gradient tensor.

[2 marks]

(ii) The strain energy of the material is given by  $\mathcal{W}(\mathbf{c}, \mathbf{a} \otimes \mathbf{a})$  and must remain unchanged if the material and the fibres are simultaneously rotated about any axis in the undeformed configuration. Explain why this leads to the restriction

$$\mathcal{W}(\mathbf{c}, \mathbf{a} \otimes \mathbf{a}) = \mathcal{W}(\mathbf{Q}\mathbf{c}\mathbf{Q}^T, \mathbf{Q}\mathbf{a} \otimes \mathbf{a}\mathbf{Q}^T), \quad (1)$$

for any proper orthogonal tensor  $\mathbf{Q}$ . Here  $\mathbf{c} = \mathbf{F}^T\mathbf{F}$  is the Cauchy-Green deformation tensor.

[3 marks]

(iii) If the strain energy is written as a function of the five invariants

$$I_1 = \text{trace}(\mathbf{c}), \quad I_2 = \frac{1}{2} \{[\text{trace}(\mathbf{c})]^2 - \text{trace}(\mathbf{c}^2)\}, \quad I_3 = \det(\mathbf{c}), \quad I_4 = \mathbf{a} \cdot \mathbf{c}\mathbf{a}, \quad I_5 = \mathbf{a} \cdot \mathbf{c}^2\mathbf{a},$$

show that the constraint (1) would be satisfied.

[6 marks]

4. An incompressible, hyperelastic solid sphere has undeformed radius 1. The sphere undergoes a deformation such that it remains spherical with a twist (rotation about an axis passing through its centre) that varies with distance from the centre of the sphere. The strain energy function of the solid material is given by

$$\mathcal{W} = (I_1 - 3) + (I_2 - 3),$$

where  $I_1$  and  $I_2$  are the first and second strain invariants.

(i) Explain why the radius of the sphere cannot change under the imposed deformation.

[2 marks]

(ii) Write down the deformed position in components in a global Cartesian coordinate system as a function of the undeformed position described using spherical polar coordinates ( $\xi^1 = r, \xi^2 = \theta, \xi^3 = \phi$ ). The global coordinate system is chosen so that the axis of rotation is the  $z$  axis. You may assume that the twist is given by a function of the form  $\Phi = \phi + f(r)$ , where  $\Phi$  is the azimuthal angle in the deformed configuration.

[2 marks]

(iii) Hence, compute the three strain invariants corresponding to this deformation.

[10 marks]

(iv) Compute the component of the stress tensor  $T^{13}$  and find a condition on  $f$  which ensures that  $T^{13} = 0$ . Give a description of the deformation in this case.

[4 marks]

**You may use** the fact that in spherical polar coordinates the position is given by

$$\mathbf{r} = r \sin \theta \cos \phi \mathbf{e}_x + r \sin \theta \sin \phi \mathbf{e}_y + r \cos \theta \mathbf{e}_z,$$

and the only non-zero Christoffel symbols are

$$\begin{aligned} \Gamma_{12}^2 = \Gamma_{21}^2 = \Gamma_{13}^3 = \Gamma_{31}^3 = \frac{1}{r}, \quad \Gamma_{23}^3 = \Gamma_{32}^3 = \frac{\cos \theta}{\sin \theta}, \\ \Gamma_{22}^1 = -r, \quad \Gamma_{33}^1 = -r \sin^2 \theta, \quad \Gamma_{33}^2 = -\cos \theta \sin \theta. \end{aligned}$$

5. A one-dimensional bar of thermoelastic material, initially of unit density, is stretched from its undeformed length of 1 to a length  $\lambda$ . The unidirectional Cauchy stress is given by a scalar quantity  $P$ . The fact that the problem is entirely one-dimensional reduces all tensors to scalar quantities. The Helmholtz free energy takes the form  $\Psi(\lambda, \Theta)$ .

(i) Explain why the second Piola–Kirchhoff stress tensor is given by  $S = \lambda P$  and find an expression for the Green–Lagrange strain,  $E$ .

[3 marks]

(ii) Use the Clausius–Duhem inequality to show that

$$P = \rho \frac{\partial \Psi}{\partial \lambda}, \quad \eta = -\frac{\partial \Psi}{\partial \Theta}.$$

[5 marks]

(iii) Hence show that

$$\left. \frac{\partial(P/\rho)}{\partial \Theta} \right|_{\lambda} = \left. \frac{\partial S}{\partial \Theta} \right|_{\lambda} = - \left. \frac{\partial \eta}{\partial \lambda} \right|_{\Theta}.$$

[5 marks]

(iv) Show that for an isentropic material (total entropy is fixed)

$$dS = \left[ \frac{\partial S}{\partial E} + \frac{1}{\lambda} \left( \frac{\partial S}{\partial \Theta} \right)^2 \right] dE,$$

and interpret the result in terms of the elastic and thermal components.

[5 marks]

Recall that the differential (infinitesimal change) of a function of two variables  $A(x, y)$  is such that

$$dA = \frac{\partial A}{\partial x} dx + \frac{\partial A}{\partial y} dy.$$

6. An incompressible, generalised Oldroyd B fluid has the constitutive relationship

$$\mathbf{T} = -P\mathbf{I} + 2\mu\mathbf{D} + G\mathbf{A},$$

where the tensor  $\mathbf{A}$  satisfies

$$\mathbf{A}^\nabla = -\frac{1}{\tau}(\mathbf{A} - \mathbf{I});$$

here,  $P$  is the fluid pressure and  $\mu$ ,  $G$  and  $\tau$  are constants. The upper-convected derivative is defined by

$$\mathbf{A}^\nabla = \frac{D\mathbf{A}}{Dt} - \mathbf{L}\mathbf{A} - \mathbf{A}\mathbf{L}^T,$$

where  $\mathbf{L}$  is the Eulerian velocity gradient tensor and  $\mathbf{D}$  is the symmetric part of  $\mathbf{L}$ .

(i) Confirm that the constitutive relationships are objective.

[7 marks]

**You may assume** that the Cauchy stress  $\mathbf{T}$  is objective; that the deformation gradient tensor,  $\mathbf{F}$ , transforms as  $\mathbf{F}^* = \mathbf{Q}\mathbf{F}$  and  $\dot{\mathbf{F}} = \mathbf{L}\mathbf{F}$ , where  $\mathbf{Q}$  is an orthogonal matrix that expresses the relative rotation between observers.

A steady two-dimensional shear flow in Cartesian coordinates is given by  $\mathbf{V} = (\epsilon Y, 0)$ , where  $\epsilon$  is the constant shear rate and  $X$  and  $Y$  are the Cartesian coordinates.

(ii) Find the Cauchy stress components  $T_{XX}$ ,  $T_{YY}$ ,  $T_{XY}$  of an Oldroyd B fluid subject to this flow and find a condition on the fluid pressure which ensures that Cauchy's equation is satisfied.

[9 marks]

(iii) Calculate the normal stress difference  $T_{XX} - T_{YY}$  for the flow and hence determine whether the fluid is Newtonian.

[2 marks]

FORMULA SHEET

- For a general (Lagrangian) coordinate system  $\xi^i$ :

$$\mathbf{g}_i = \frac{\partial \mathbf{r}}{\partial \xi^i}, \quad \mathbf{g}_i \cdot \mathbf{g}^j = \delta_i^j, \quad g_{ij} = \mathbf{g}_i \cdot \mathbf{g}_j, \quad g = \det(g_{ij}).$$

$$\mathbf{G}_i = \frac{\partial \mathbf{R}}{\partial \xi^i}, \quad \mathbf{G}_i \cdot \mathbf{G}^j = \delta_i^j, \quad G_{ij} = \mathbf{G}_i \cdot \mathbf{G}_j, \quad G = \det(G_{ij}).$$

- For a scalar field  $f(\mathbf{x})$  and vector field  $\mathbf{u}(\mathbf{x})$

$$\nabla f = \mathbf{g}^i \frac{\partial f}{\partial \xi^i}, \quad \text{div } \mathbf{u} = \frac{1}{\sqrt{g}} \frac{\partial (u^i \sqrt{g})}{\partial \xi^i}, \quad \text{curl } \mathbf{u} = \epsilon^{ijk} u_j |_{,i} \mathbf{g}_k.$$

- The material derivative in general coordinates is

$$\frac{DU^i}{Dt} = \frac{\partial U^i}{\partial t} + V^j U^i |_{,j},$$

where  $\mathbf{V}$  is the velocity of the continuum and

$$U^i |_{,j} = U^{i,j} + \Gamma_{jk}^i U^k,$$

where  $\Gamma_{jk}^i$  are the Christoffel symbols for the chosen coordinate system in the deformed configuration.

- The deformation gradient tensor  $\mathbf{F} = \nabla_{\mathbf{r}} \mathbf{R}$  has components Cartesian coordinates given by

$$F_{IJ} = \frac{\partial X_I}{\partial x_j}.$$

The determinant of  $\mathbf{F}$  is denoted by  $J$ .

- The Eulerian velocity gradient tensor,  $\mathbf{L}$ , has components in Cartesian coordinates given by

$$L_{IJ} = \frac{\partial V_I}{\partial X_J}.$$

- The deformation rate tensor,  $\mathbf{D}$  and spin tensor,  $\mathbf{W}$  are defined by

$$\mathbf{D} = \frac{1}{2} (\mathbf{L} + \mathbf{L}^T), \quad \mathbf{W} = \frac{1}{2} (\mathbf{L} - \mathbf{L}^T).$$

- Cauchy's equation in the usual notation in components in general coordinates  $\xi^i$  is

$$T^{ji} |_{,j} + \rho F^i = \rho \ddot{U}^i = \rho \frac{DV^i}{Dt}, \quad \text{where } T^{ji} |_{,j} = T^{j,i} + \Gamma_{jr}^j T^{ri} + \Gamma_{jr}^i T^{jr}.$$

- The material derivative of the determinant of the deformation gradient tensor is

$$\frac{DJ}{Dt} = J \nabla_{\mathbf{R}} \cdot \mathbf{V}.$$

- The Reynolds Transport theorem states that

$$\frac{d}{dt} \int_{\Omega_t} \phi \, d\mathcal{V}_t = \int_{\Omega_t} \left( \frac{D\phi}{Dt} + \phi \nabla_{\mathbf{R}} \cdot \mathbf{V} \right) d\mathcal{V}_t,$$

where  $\Omega_t$  is a material volume,  $\phi$  is a scalar field and  $\mathbf{V}$  is the velocity of the continuum.

- For a Cartesian line element  $dX_I$  in the deformed configuration

$$\frac{DdX_I}{Dt} = V_{I,K} dX_K,$$

where  $V_I$  is the  $I$ -th Cartesian component of the velocity.

- Nanson's relation states that

$$dA_{\bar{i}} = J \frac{\partial \xi^j}{\partial \chi^{\bar{i}}} da_j,$$

where  $\xi^j$  are the Lagrangian coordinates,  $\chi^{\bar{i}}$  are the Eulerian coordinates,  $J$  is the determinant of the deformation gradient tensor,  $d\mathbf{A}$  is an area element in the deformed configuration and  $d\mathbf{a}$  is an area element in the undeformed configuration.

- The Green–Lagrange strain tensor is defined by

$$\gamma_{ij} = \frac{1}{2} (G_{ij} - g_{ij}).$$

- The strain invariants are defined by

$$I_1 = g^{ij} G_{ji}, \quad I_2 = \frac{1}{2} (I_1^2 - g^{ir} g^{js} G_{ij} G_{rs}), \quad I_3 = G/g,$$

where  $g = \det(g_{ij})$  and  $G = \det(G_{ij})$

- A hyperelastic material is described by a strain energy function  $\mathcal{W}(I_1, I_2, I_3)$  such that

$$T^{ij} = PG^{ij} + Ag^{ij} + BB^{ij},$$

where

$$A = \frac{2}{\sqrt{I_3}} \frac{\partial \mathcal{W}}{\partial I_1}, \quad B = \frac{2}{\sqrt{I_3}} \frac{\partial \mathcal{W}}{\partial I_2}, \quad P = 2\sqrt{I_3} \frac{\partial \mathcal{W}}{\partial I_3},$$

and  $B^{ij} = [I_1 g^{ij} - g^{ir} g^{js} G_{rs}]$ .

- The physical components of the stress tensor are given by  $\sigma_{(ij)} = T^{ij} \sqrt{G_{jj}/G^{ii}}$  (no summation).
- The body stress tensor  $T^{ij}$  and second Piola–Kirchhoff stress tensor  $s^{ij}$  are related by the expression  $JT^{ij} = s^{ij}$ .
- The first law of thermodynamics can be written as

$$\rho \frac{D\Phi}{Dt} = \mathbb{T} : \mathbb{D} + \rho B - \nabla_{\mathbf{R}} \cdot \mathbf{Q} + \mathcal{W}_e,$$

where  $\mathcal{W}_e$  is any additional non-thermomechanical rates of work.



- The second law of thermodynamics for continuum mechanics can be written as

$$\rho\dot{\eta} \geq -\nabla_{\mathbf{R}} \cdot \left( \frac{\mathbf{Q}}{\Theta} \right) + \rho \frac{B}{\Theta}.$$

- The Clausius–Duhem inequality is

$$-\rho\dot{\Psi} - \rho\eta\dot{\Theta} - \frac{1}{\Theta}\mathbf{Q} \cdot \nabla_{\mathbf{R}}\Theta + \mathbb{T} : \mathbb{D} \geq 0,$$

where  $\Psi = \Phi - \eta\Theta$ ; or (in the Lagrangian viewpoint)

$$-\rho_0\dot{\psi} - \rho_0\eta_0\dot{\theta} - \frac{1}{\theta}\mathbf{q} \cdot \nabla_r\theta + s^{ij} : \dot{\gamma}_{ij} \geq 0,$$

where  $\psi = \Psi$ .

- The most general transformation of position and time between observers in Euclidean space is

$$\mathbf{R}^*(t^*) = \mathbf{Q}(t)\mathbf{R}(t) + \mathbf{C}(t), \quad t^* = t - a,$$

where  $\mathbf{Q}$  is an orthogonal matrix,  $\mathbf{C}$  is a translation vector and  $a$  is a constant time shift.

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END OF EXAMINATION PAPER